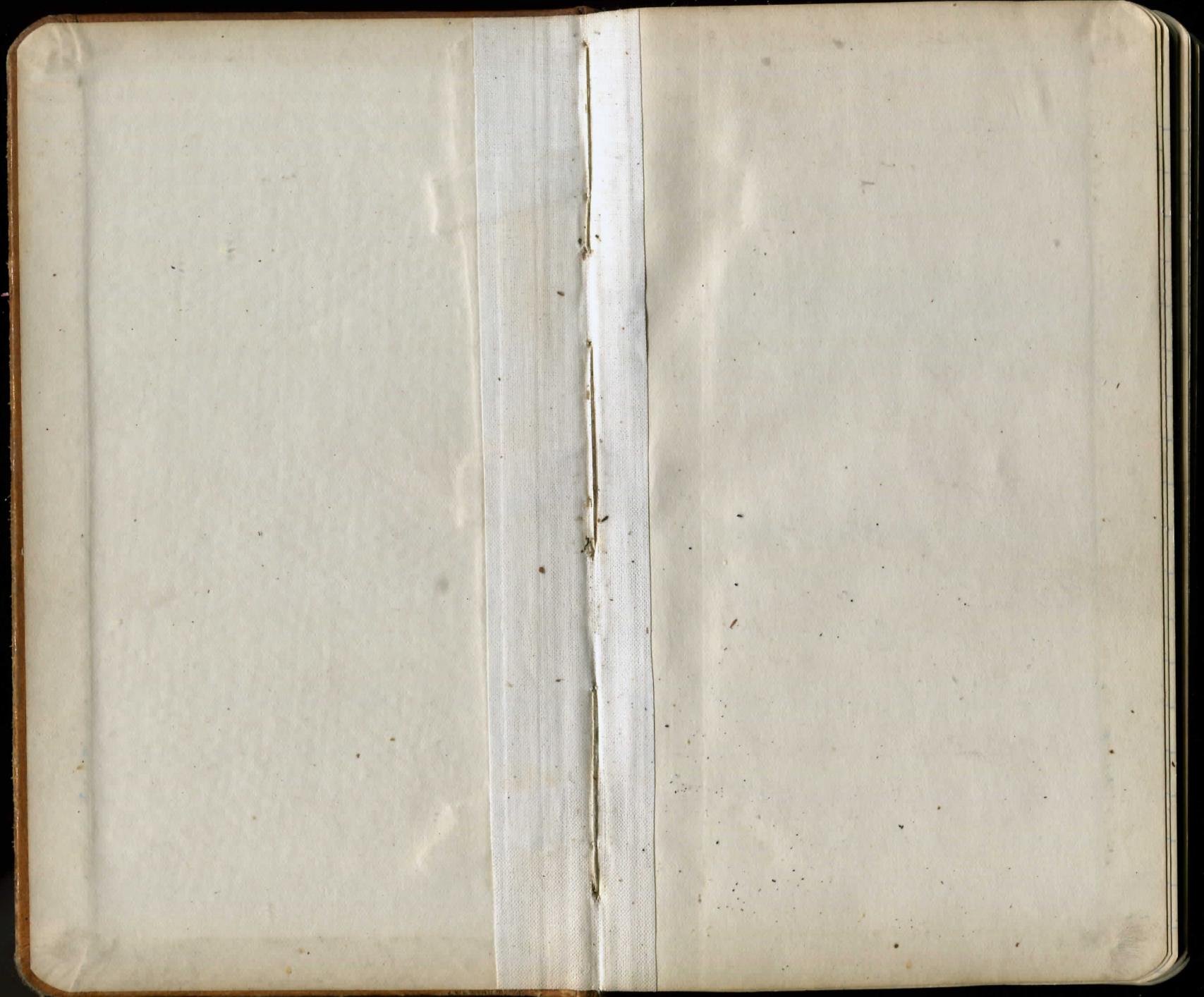
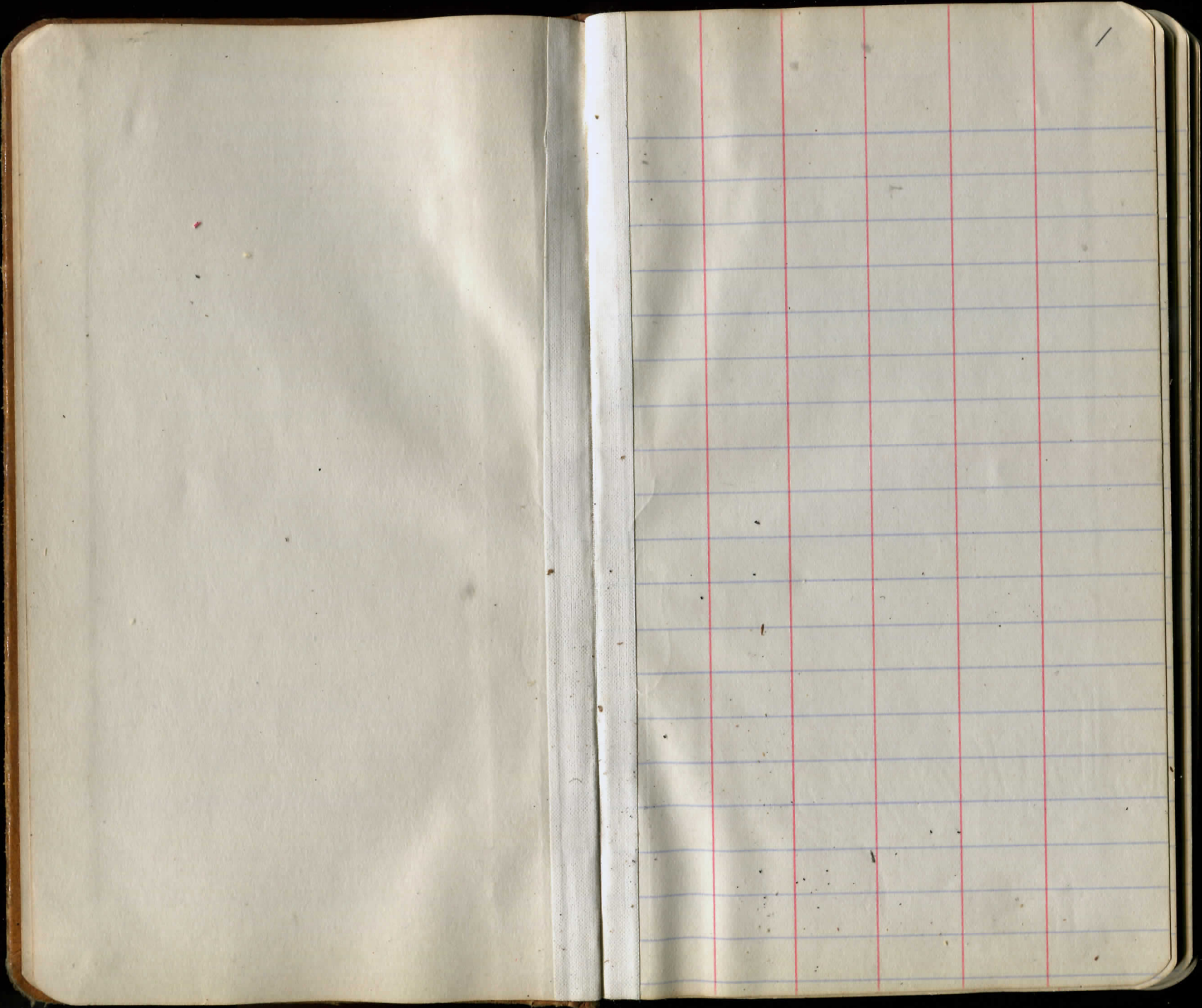


*PHELPS CREEK
COUNTY DITCH*

LEVEL BOOK.

No. 410





Elev of B.M. on Middlefield Tower
Hall 1141.33

7/25

F. H. Zehmayer
P. Hanna

warm - cloudy

5

Preferable to use

Sta	B.S. +	H T	F.S -	Elev.
B.M.				1141.33
T.P.	3.58	1144 91	1.48	1143.93
T.P.	9.55	1152 98	1.91	1151.07
T.P.	11.47	1162 54	0.47	1162.07
T.P.	7.03	1169 10	1.94	1167.16
T.P.	4.79	1171 95	5.70	1166.25
T.P.	7.64	1173 89	3.53	1170.36
T.P.	1.69	1172 05	2.42	1169.63
T.P.	0.21	1169 84	8.90	1160.94
T.P.	0.26	1161 20	7.45	1153.75
B.M.		1161 20	6.79	1154.41
T.P.	0.50	1154 25	5.70	1148.55
T.P.	0.51	1149 06	10.15	1138.91
T.P.	4.15	1143 06	7.66	1135.46

Tablet on Middlefield Town Hall.

+ on stone 8.6 N.W. of N.W. corner of Sugar House
of Joe Johnson

7/23/44

warm - cloudy

7

	F.S.	H.I.	B.S.	Elev
B.M.				1141.33
T.P.	1.14	1144.57	324	1143.43
T.P.	1.45	1152.52	9.09	1151.07
T.P.	0.22	1161.59	10.52	1161.37
T.P.	1.95	1169.09	7.72	1167.14
T.P.	6.16	1172.21	5.07	1166.05
T.P.	3.43	1173.78	7.73	1170.35
T.P.	2.82	1172.42	2.07	1169.60
T.P.	8.91	1169.80	0.20	1164.89
T.P.	7.53	1161.21	0.32	1153.68
B.M.	6.86			1154.35
T.P.	6.71	1155.16	1.48	1148.95
T.P.	10.39	1149.20	0.75	1138.81
T.P.	6.85	1142.14	3.33	1135.29
	6.1			1136.00

+ on stone 8.6 N.W. of N.W. Cor. of Sugar House
of Joe Johnson

of 3 to 0
about 200' W, on prop. line (on ground)

Sta	B.S.	I.	F.S.	Elev.				
T.P.	2.12	1137	52	1135.40				
0			3.7	1133.8	-1.2	-0.5	-0.8	0.0
+25			4.9	1132.6	22.0	15.0	8.0	5.0
+49			5.0	1132.5				
+57			4.0	1133.5				
+70			4.6	1132.9	+0.1	0.0	-1.0	-1.0
+80			3.0	1134.5	4.0	0.0	2.0	9.0
1			5.2	1132.3				
+50			5.2	1132.3	+1.5	0.0	+0.1	+0.4
+55			5.6	1131.9	7.0	0.0	3.0	8.0
+90			5.3	1132.2				
2			4.8	1132.7	-1.5	0.0	-0.5	
+25			5.7	1131.8	10.0	0.0	10.0	
+50			6.3	1131.2	+0.5	0.0	-2.0	-1.5
T.P.	3.36	1134	69	1131.33	8.0	0.0	1.0	5.0
3			3.6	1131.1				
+12			4.2	1130.5	-0.2	0.0	0.0	
+15			2.5	1132.2	10.0	0.0	10.0	
+20			3.6	1131.1				

Sta	B.S.	H I	F.S	Elev
3+70	1134 09		3.9	1130.8
+71			4.9	1129.8
+77			5.0	1129.7
+78			3.5	1131.2
4			3.9	1130.8
5			4.4	1130.3
6			5.0	1129.7
+70			6.3	1128.4
+71			5.5	1129.2
7			5.2	1129.5
T.P.	2.89	1132 54	5.04	1129.65
8			3.1	1129.4
9			3.8	1128.7
10			4.7	1127.8
11			5.5	1127.0
+10			6.1	1126.4
+15			7.3	1125.2
+20			5.8	1126.7

L+

L

F+

11

10.0	00	00	
-0.5	00	00	-0.5
10.0	00	4.0	10.0
-0.2	00	+0.2	
10.0	00	10.0	
0.0	00	+0.2	
10.0	00	10.0	
-0.2	00	+0.1	
15.0	00	10.0	
-0.3	00	+0.3	
15.0	00	15.0	
-0.3	00	+0.3	
15.0	00	15.0	
-0.6	00	-0.1	
15.0	00	15.0	

Sta B.S. H I F.S. Elev.

12 1132 54 6.9 1125.6

+10 7.6 1124.9

+18 6.2 1126.3

+80 7.5 1125.0

+85 6.6 1125.9

T.P. 4.45 1130 10 6.89 1125.65

13 4.7 1125.4

+30 4.7 1125.4

+35 5.1 1125.0

+40 4.1 1126.0

+85 4.5 1125.6

+90 5.6 1124.5

14 5.2 1124.9

+50 5.4 1124.7

+55 6.0 1124.1

+61 5.2 1124.9

+73 5.2 1124.9

+80 6.0 1124.1

+90 6.0 1124.1

Lt.

2

Rt.

+0.7 +0.2 -0.6
20.0 15.0 10.0

-0.5 +1.3 +1.8
10.0 15.0 20.0

+0.8 -0.3 -0.4 0.0 -0.1 +0.2 +0.5 -0.8
15.0 10.0 6.0 0.0 10.0 15.0 20.0 25.0

+1.0 +0.6 0.0 -0.1 +1.0
15.0 5.0 0.0 10.0 15.0

Sta B.S. H I. F.S Elev.

15 1130 10 5.9 1124.2

+12 6.2 1123.9

+25 4.7 1125.4

+50 5.8 1124.3

T.P. 5.15 1130 04 5.21 1124.89

16 5.5 1124.5

+10 6.2 1123.8

+18 5.1 1124.9

17 5.0 1125.0

+36 5.8 1124.2

+40 6.4 1123.6

+60 6.2 1123.8

+85 6.6 1123.4

+90 5.3 1124.7

18 5.0 1125.0

T.P. 5.24 1129 43 5.85 1124.19

19 5.4 1124.0

+80 5.5 1123.9

Lt.

R

Ft.

+0.6 +0.9 +0.7 0.0 -0.3 0.0 +1.0
15.0 10.0 4.0 0.0 10.0 15.0 20.0

-0.6 -0.8 -0.6 0.0 +0.3
20.0 14.0 7.0 0.0 15.0

+0.5 0.0 -0.6 -2.6
15.0 0.0 10.0 15.0

+0.4 0.0 -1.0
15.0 0.0 15.0

-0.1 0.0 +0.4
0.0 15.0

Sta	B.S.	H.I.	F.S	Elev.
20		1129 43	4.3	1125.1
21			5.6	1123.8
T.P.	4.67	1129 28	4.82	1124.61
22			5.9	1123.4
+30			6.2	1123.1
+40			5.9	1123.9
23			5.3	1124.0
B.M.			4.50	1124.78
24			5.0	1124.3
25			6.6	1122.7
+20			7.7	1121.6
+25			8.4	1120.9
+37 -10			4.9	1124.4
0+47			4.9	1124.4
			3.7	1125.6

Lt. R

$\frac{00}{15.0}$ $\frac{00}{00}$ -0.2
15.0 15.0

$\frac{00}{15.0}$ $\frac{00}{00}$ +0.2
15.0 15.0

$\frac{00}{15.0}$ $\frac{00}{00}$ -0.1 +0.2
15.0 15.0

-0.3 $\frac{00}{00}$ -0.7
 $\frac{00}{15.0}$ 15.0

2 10d. Nails in N.E. root of 30" Maple tree
150' West of Rd in front of W. King's house
30' E of Sta 23.

+0.6 $\frac{00}{00}$ +0.3 $\frac{00}{00}$
15.0 15.0 15.0

-0.1 $\frac{00}{00}$ +0.2
15.0 15.0

On S. abutment to bridge (and top of floor)
N. of Sta 25+47 (10" joists)

7/29/14 F. Zethmayer cloudy-cool.
R. Hanna

Sta	B.S.	H.I.	F.S.	Elev
B.M.	329	112807		112478
25+47			3.7	1124.7
+62			2.8	1125.3
+80			7.0	1121.1
26			5.2	1122.9
27			5.5	1122.6
T.P.	310	112663	4.54	1123.53
28			4.0	1122.6
29			5.8	1120.8
30			7.2	1119.4
T.P.	445	112587	5.21	1121.42
31			5.3	1120.6
32			5.2	1120.7
33			5.9	1120.0
34			6.0	1119.9
T.P.	456	112476	5.67	1120.20

Lt K Ft

+ on Maple tree

-2.4	+0.6	0.0	+0.1	-2.5
15.0	8.0	0.0	15.0	20.0
edge of bridge	+0.3	0.0	-3.1	-3.9
	15.0	0.0	8.0	15.0
	+0.2	0.0	+1.0	
	15.0	0.0	15.0	
	-1.8	-1.1	0.0	+2.8
	15.0	4.0	0.0	15.0
-0.8	-1.5	-2.1	-1.3	-0.1
15.0	7.0	5.5	4.0	1.0
				0.0
				+0.3
				15.0
-0.4	-0.5	-1.7	-3.3	-0.3
15.0	10.0	7.0	3.0	1.0
				0.0
				+0.1
				6.0
				15.0
+0.7	+0.8	0.0	-0.8	-0.9
15.0	11.0	0.0	3.5	1.0
				0.0
				+0.7
				15.0
+1.6	+2.4	+1.5	+1.0	-0.1
15.0	7.0	6.0	3.0	2.0
				0.0
				+1.2
				2.0
				5.0
				6.0
				15.0
+1.2	+1.9	+0.4	0.0	-1.3
15.0	5.0	3.0	0.0	3.0
				6.0
				10.0
				15.0
+0.2	+0.6	0.0	-1.3	-1.0
15.0	1.0	0.0	4.0	10.0
				15.0
+0.5	0.0	0.0	+0.4	-0.4
15.0	8.0	0.0	7.0	11.0
				18.0
+0.6	-0.4	0.0	+0.5	-0.6
20.0	15.0	0.0	9.0	14.0
				2.1

95 94
29

Sta	B.S.	H. I.	F.S.	Elev
35		1124 76	5.3	1119.5
B.M.			2.60	1122.16
X sec. of Rd. E. end of bridge			1.60	1123.2
20' E of end of ...			3.1	1121.7
X Sec. of Rd. W. end of bridge			1.7	1123.1
20' W of end of ...			2.9	1121.9
B.M. 225	1124 41			1122.16
			0.9	1123.5
(P.M. warm)			5.54	1118.87
360			4.3	1120.1
37			4.5	1119.9
38			5.5	1118.9
39			5.1	1119.3
T.P. 334	1123 48		4.27	1120.14
40			4.4	1119.1
41			5.4	1118.1

Lt. # Ft

+0.7 0.0 +0.3 -0.2
 15.0 15.0 15.0 15.0
 + on stone in S.E. cor of S. abutment to bridge
 Sta 35+50

-2.6	0.0	0.0	-0.1	-2.9	-4.0
9.0	6.0		6.5	10.0	17.0
-1.7	-1.2	+0.2	0.0	+0.2	-1.5
14.0	8.0	6.5		7.0	10.0
-4.1	-2.6	-2.7	+0.3	0.0	-0.2
16.0	11.0	8.0	6.5	0.0	6.5
				9.0	14.0

on bridge
 On bridge floor E end
 N. end of bridge bed of stream

+0.2	0.0	+0.3
15.0	0.0	15.0
-0.7	0.0	-0.4
15.0	0.0	15.0
-0.1	0.0	-0.1
15.0	0.0	15.0
-0.5	0.0	-0.4
15.0	0.0	15.0

+0.4	0.0	-0.1
15.0	0.0	15.0
+0.8	+0.1	0.0
15.0	12.0	0.0
		+0.4
		15.0

Sta	BSI	H.I.	F.S.	Elev
42		1123 48	5.2	1118.3
43			5.8	1117.7
T.P.	5.37	1124 01	4.84	1118.64
44			6.8	1117.2
45			6.0	1118.0
+25			6.0	1119.0
+40			3.6	1120.4
46			4.1	1119.9
47			3.9	1120.1
T.P.	2A2	1123 25	3.18	1120.83
48			4.6	1118.7
B.M.			3.19	1120.06
49			5.2	1118.1
T.P.	3.94	1123 32	3.87	1119.38
50			5.4	1117.9
51			5.2	1118.1

Used

-0.4	00	-0.4	other notes.
15.0	00	15.0	
+1.8	+1.3	+0.3	00
15.0	10.0	6.0	00
			18.0

+2.0	+0.4	00	+1.0
17.0	12.0	00	15.0

+0.4	00	00
15.0	00	15.0

+1.6	+1.7	+1.0	00	-0.7
15.0	12.0	6.0	00	15.0

+0.4	00	-1.1	-3.2
15.0	00	9.0	15.0

+0.1	-0.4	00	+0.4
15.0	12.0	00	15.0

0.0	00	-0.3
15.0	00	15.0

-0.2	00	+0.2
15.0	00	15.0

Nail in W. root of 30" Red Oak + 25' E of Sta (48+40)

00	00	00
15.0	00	15.0

00	00	0.6
15.0	00	15.0

+0.1	00	-0.1
15.0	00	15.0

Sta	B.S.	I.T.	F.S.	Elev
52	1123	32	3.7	1119.6
+55			2.9	1120.4
53			4.1	1119.2
T.P.	1.83	1121	71	3.44 1119.88
54			4.3	1117.4
+54			5.4	1116.3
+60			4.3	1117.4
55			4.2	1117.5
56			5.4	1116.3
T.P.	2.62	1120	30	4.03 1117.68
57			4.1	1116.2
58			5.2	1115.1
59			4.9	1115.4
+7			4.7	1115.6
+8			5.7	1114.6
+22			6.0	1114.3
+36			5.6	1114.7
+38			4.8	1115.5

Lt. ♀ Ft.

-0.6 -0.7 0.0 -0.8 -0.8
15.0 3.0 0.0 4.0 15.0

-1.4 -0.5 0.0 -0.2
15.0 12.0 0.0 15.0

-0.1 0.0 -0.2
15.0 0.0 15.0

0.0
0.0

0.0 -0.4 0.0 -0.5 -1.2
15.0 3.0 0.0 4.0 15.0

-0.9 0.0 -1.2 -1.6
15.0 0.0 4.0 15.0

0.0 0.0 -0.1 -0.6
15.0 0.0 10.0 15.0

-0.2 0.0 -0.1 +0.5
15.0 0.0 12.0 15.0

+0.1 0.0 -0.2 -1.4 -1.3 0.0
15.0 0.0 2.0 6.0 15.0 17.0

200' longer
on New Line

Sta	B.S.	H.I.	F.S.	Elev
60		1120.30	5.5	1114.8
T.P.	3.03	1118.19	5.14	1115.16
61			4.7	1113.5
+85			4.0	1114.2
62			5.0	1113.2
63			5.7	1112.5
T.P.	4.75	1118.91	4.03	1114.16
B.M.?	3.53	1119.27	3.28	1115.99
T.B.M.			3.17	1115.74
T.P.	3.48	1119.22		
64			7.1	1112.1
65			7.7	1111.5
+50			7.7	1111.5

Lt 2 Rt.

	-0.3	0.8	0.0	-1.5	-0.1	-0.5
	15.0		0.4	6.0	9.0	15.0
+0.7	0.0	-0.2	0.0	+0.5		
16.0	13.0	4.0		15.0		
	-0.3	0.0	-0.6	-2.4	-1.3	-2.3
	15.0	10.0	1.0	4.0	6.0	8.0
	+0.1	0.0	-0.5	-1.7	-0.5	+0.2
	15.0	20.0	4.0	10.0	15.0	20.0
+0.9	-0.5	-1.3	0.0	-0.7	-0.4	
14.0	14.0	9.0	20.0	10.0	15.0	

2-8d Nails in E roof of twin white elm tree,
5' E of fence running N. of Sta 60.

Arch root to W. of 12" Elm, E bank 62 + 45

→ +1.0 +3.2 +1.9 +0.5 0.0 +2.3 +2.1 64
 15.0 9.0 7.0 4.0 0.0 1.0 15.0

→ +3.6 +2.7 +1.9 +0.5 0.0 +0.5 +2.7 +1.8 65
 17.0 12.0 4.0 2.0 0.0 3.0 2.0 15.0

→ +0.7 +2.0 +1.9 +0.4 0.0 +1.9 +1.7 +50
 15.0 11.0 5.0 2.0 0.0 11.0 15.0

Friday P.M. F. H. + D. April 9th 1915

BS+	IS	FS-	ℓ. Ter.
B.M.			1115.28
+3.67	1118.92		
⁸ 6.6		8.4	1110.5
⁹ 6.8		8.5	1110.4
+5.0		8.5	1110.4
EXT 6'			
+70.4		7.2	1111.7
T.P.		-7.38	1111.54
+3.00	1114.54		
⁷⁰ 68		3.60	1110.9
+5.0		4.30	1110.2
⁷¹ 6.9		3.90	1110.6
+5.0		4.90	1109.6
+7.5		5.70	1108.8
⁷² 7.0		4.80	1109.7
+2.0		-3.7	1110.8
EXT 10'			
⁷³ 7.1		3.4	1111.1
+4.0		4.9	1109.6
³ 7.1 + 7.2		2.00	1112.54

note "+" indicates height above & Elev.
 "-" " " " below " "

Sections are averaged for correct calculations

Left & Right

$$\begin{array}{r} +1.0 \\ 70.0 \end{array} \quad \begin{array}{r} +.7 \\ 3.5 \end{array} \quad \begin{array}{r} +2.0 + 2.00 \\ 6.0 \quad 10.00 \end{array}$$

$$\begin{array}{r} +1.0 \\ 10.0 \end{array} \quad \begin{array}{r} +1.0 \\ 7.0 \end{array} \quad \begin{array}{r} +0.7 \\ 1.0 \end{array}$$

$$\begin{array}{r} +1.0 \\ 7.7 \times 10. \end{array} \quad \begin{array}{r} +0.5 \\ 3.0 \end{array} \quad \begin{array}{r} +0.6 \\ 1.0 \end{array}$$

$$\begin{array}{r} +1.1 \\ 18. \end{array} \quad \begin{array}{r} -0.4 \\ 6.0 \end{array} \quad \begin{array}{r} -0.6 \\ 5.0 \end{array} \quad \begin{array}{r} -1.3 \\ 6.0 \end{array} \quad \begin{array}{r} -1.1 \\ 10.0 \end{array} \quad \begin{array}{r} -0.6 \\ 13.0 \end{array}$$

Top of stake "68"

$$\begin{array}{r} +0.2 \\ 10.0 \end{array} \quad \begin{array}{r} -0.4 \\ 4.0 \end{array} \quad \begin{array}{r} -0.8 \\ 10.0 \end{array}$$

$$\begin{array}{r} +0.8 \\ 10. \end{array} \quad \begin{array}{r} -3 \\ 10. \end{array} \quad \begin{array}{r} -0.7 \\ 10. \end{array}$$

$$\begin{array}{r} +0.8 \\ 10.0 \end{array} \quad \begin{array}{r} -0.7 \\ 7.0 \end{array} \quad \begin{array}{r} +0.5 \\ 10.0 \end{array}$$

$$\begin{array}{r} +1.0 \\ 10.0 \end{array} \quad \begin{array}{r} 0.0 \\ 10.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ 10.0 \end{array} \quad \begin{array}{r} 0.0 \\ 10.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ 10 \times 15 \end{array} \quad \begin{array}{r} +0.6 \\ 7.0 \end{array} \quad \begin{array}{r} +1.8 \\ 7 \frac{1}{2} \times 10.0 \end{array}$$

$$\begin{array}{r} -2.0 \\ 18. \end{array} \quad \begin{array}{r} -0.3 \\ 10.0 \end{array}$$

$$\begin{array}{r} -1.2 \\ 10 \times 20.0 \end{array} \quad \begin{array}{r} -0.4 \\ 10 \times 15 \end{array}$$

$$\begin{array}{r} 0.0 \\ 10 \times 20. \end{array} \quad \begin{array}{r} +0.6 \\ 10 \times 15 \end{array}$$

average banks 5-0° R + L

	+B.S.	H ₂	± F.S.	Elev.
7 ⁴		1114.54	5.3	1109.2
+75-			6.2	1109.3
7 ⁵			5.2	1109.3
+50			3.8	1110.7
7 ⁶			5.1	1109.4
+70			4.1	1110.4
7 ⁷			3.0	1111.5
T.P.			-2.65	1111.89

+2.73 1114.62

7 ⁸			6.1	1109.5
+69.7			4.5	1110.1
B.M.			-2.85	1111.77
7 ⁹			5.2	1109.4
+20			4.6	1110.0
+80			5.4	1109.2
+90		water 1.2 deep	6.8	1107.8
80			4.9	1109.7
+50			4.8	1109.9
+75		w. 2.0 deep	8.10	1106.52

Left	±	RT.
$\frac{-0.7}{10 \times 15.0}$	0	$\frac{+1.0}{8.0} \frac{+2.0}{10 \times 12.0}$
$\frac{+0.5}{10.0}$	0	$\frac{+0.6}{10.0}$
$\frac{+0.2}{10 \times 12.0}$	0	$\frac{+0.7}{8.0} \frac{+1.3}{10.0}$
$\frac{+0.5}{10.0}$	0	$\frac{-1.4}{4.0} \frac{-1.6}{12.0}$
$\frac{+0.4}{12.0} \frac{-0.4}{5.0}$	0	$\frac{+0.2}{4.0} \frac{+1.8}{5 \times 10.0}$
$\frac{+1.7}{10.0} \frac{+1.1}{5.0}$	0	$\frac{-1.5}{10 \times 15.0}$
$\frac{+0.3}{15.0}$	0	$\frac{-1.5}{6.0} \frac{-3.0}{15.0}$

stake "75" ± on top

Hickory

$\frac{0.0}{10.0}$	0	$\frac{+1.8}{10.0}$
$\frac{+0.1}{10.0} \frac{-1.1}{5.0}$	0	$\frac{-0.3}{10.0}$
$\frac{-0.6}{10.0}$	0	$\frac{+0.4}{10.0}$
$\frac{0.0}{10.0}$	0	$\frac{0.0}{10.0}$
$\frac{+0.7}{10 \times 12.0}$	0	$\frac{0.0}{10.0}$
$\frac{0.0}{10.0}$	0	$\frac{0.0}{10.0}$
$\frac{+0.4}{10.0}$	0	$\frac{+0.5}{10.0}$
$\frac{0.0}{10.0}$	0	$\frac{0.0}{10.0}$
$\frac{+1.0}{10.0}$	0	$\frac{+1.2}{10.0}$

	+PS	11-0	24 -FS	EPers-
81			7.1	1107.5
77		1114 62		
+15			4.8	1109.8
+75			6.1	1108.5
² 80			8.3	1106.3
+60			5.3	1109.3
³ 81			4.8	1109.8
+40			6.1	1108.5
+50			7.8	1106.8
+70			6.7	1107.9
82			6.8	1107.8
83			6.3	1108.3
T.P			-6.25	1108.37
+25	+460	111297	5.8	1107.8
+35			4.8	1109.2
⁶ 84			3.3	1109.7
⁷ 85			4.1	1108.9
+35			6.3	1106.7
+45			4.9	1108.1
⁸ 86			3.3	1109.7

Left	±	Rt.
+0.5		+0.7
10.1	0	10.1
+0.3		-1.5
12	0	3.0
+1.5		-1.5
12.1	0	15.0
+1.9		0.0
15.0	0	10.0
0.0		-1.7
10.0	0	4.10
+0.4		+0.6
12.1	0	10.0
+1.2		-1.0
12.0	0	12.1
-1.1		+7.3
10.0	0	10.0
-0.4		+1.6
12.0	0	4.0
0.0		-0.7
10.0	0	2.0
+0.4		-1.0
7.0	0	10.0

Top of stakes "83"

R+L	same as ±	0
-0.3		-0.2
10.0	0	10.0
-0.2		-0.2
10	0	10
0.0		-0.2
10.0	0	10
+0.7		+0.6
10.1	0	10
-0.6		+1.5
10.0	0	10.0
-1.5		+1.4
10.0	0	10.1

11.2.97 24

trad 111297 F.S. Elevation

86+70	5.0	1108.0
87 ⁰	4.5	1108.5
+25	6.7	1106.3
+55	6.8	1106.2
87 ¹²	5.0	1108.0
88 90		
+50	6.8	1106.2
+80	5.7	1107.3
87 ⁹¹	4.4	1108.6
+85	4.9	1108.1
92 ²	7.6	1107.4
+10	5.9	1107.1
92 ³	7.2	1105.9
+10	6.4	1106.6
92 ⁴	7.7	1105.3
+95	6.2	1106.8
93 ⁵	6.3	1106.7
+45	8.0	1105.0
+60	6.3	1106.7
94 ⁶	6.2	1106.8

water 0.7 deep

water 1.1 deep

water 0.9 deep

water 0.9 deep

Left. 0 Right-

-0.6	0	-0.5
10.0	0	10.0
0.0	0	-1.0
10.0	0	10.0
0.0	0	0.0
10.0	0	10.0
-0.5	0	+1.0
10.0	0	10.0
+0.2	0	-0.8 -0.8
10.0	0	7.0 10.0
0.0	0	0.0
10.0	0	10.0
+1.4	0	-1.2
10.0	0	10.0
0.0	0	-0.4
10.0	0	10.0
0.0	0	-1.0
10.0	0	10.0
0.0	0	0.0
10.0	0	10.0
-1.0	0	0.0
10.0	0	10.0
0.0	0	+2.0
10.0	0	10.0
-0.5	0	+1.5
10.0	0	10.0
+1.0	0	+0.5
10.0	0	10.0
-1.2	0	+0.7
10.0	0	10.0
+0.8	0	-1.0
10.0	0	10.0
+1.0	0	0.0
10.0	0	10.0
+0.4	0	-1.1
10.0	0	10.0
0.0	0	0.0
10.0	0	10.0

old ang. hubs at
94 + 6-5-4 for T.P.

T.P. BS + 1112.97 -5.20 1107.77
+3.53

97
angle
+60 1111.30 5.8 1105.5
water 0.6 deep
6.6 1105.7

98
9.6 6.4 1104.9
water 1.3 deep

99
100 7.3 1104.0
water 2.5 deep

98
101 8.0 1102.7
water 2.0 deep

99
102 8.0 1103.3
water 1.6 "

105
T.P. -1.00 1110.30

+45 7.1 1104.2
water 2.0 deep

+65
Ext 5.1
104 8.2 1103.1

T.P. 6.9 1104.4
-1.00 1110.30

+0.88 1111.18

104
105 6.4 1104.8
water 1.0 deep

105 7.3 1103.9
water 0.6 deep

104 7.1 1104.1

105 5.2 1106.0
B.M. ✓ -3.245 107.935

Left \$ Right

+0.3	-	-0.4
10.0	0	10.0
0.0		-1.00
10.0	0	10.0
+1.4		-0.6
10.0	0	2.0
+0.5		-0.6
10.0	0	10.0
+3.5	+2.5	+2.0
10	8.0	10.0
+3.4	+1.3	3.5
10	2.0	8.4
+3.0	+2.6	+10.0
10.0	3.0	7.0
	4.0	10.0
		+2.0
		10.0

stone at w. end of bridge blue mark

00 1.5	+0.3	-1.2
15 12.0	8.0	8.0
	-0.4	+1.6
	10.0	10.0
+1.4	-0.6	+1.4
10.0	2.0	10.0

Bridges as above

+0.1	+0.6	+0.6	+0.1
10.0	10.0	4.0	10.0
-0.6	-0.4	+1.7	-0
10.0	0.6	10.0	
	+0.5	+0.6	
	10.0	10.0	
+0.1		+0.2	
10.0		10.0	

Hickory Tree

Lat		H. D.	Rt F.S.	Elevation
9 ¹ 10 ²	+105			
105 ² + 617		1111.18	6.4	1104.8
106 ⁸			6.9	1104.3
T.P.			-4.22	1106.96
	+1.70	1108.66		
107 ⁹			5.6	1103.1
108		water 112 deep	7.6	1101.1
109		water 1.5 deep	7.9	1100.8
110 ²			7.7	1101.0
111 ³			6.6	1102.4
112		water 1.0 deep	8.0	1100.7
113 ⁵		water 0.7 deep	7.9	1100.8
114		1.4 deep	8.7	1100.0
115 ⁷			7.9	1100.8
116 ⁴			8.4	1100.3
117 ⁹			6.8	1101.9
118			6.7	1102.0
T.P.			-6.11	1102.55
	+3.78	1106.33		
+50		✓ 53		1101.0

Left. Rt

6.3		+0.8
10.0	⊙	10.0
+0.4		+0.2
10.0	○	10.0

Erroot of hickory R. bank at 7 P.M. Friday
" 7 A.M. Sat. 1

+0.4	-0.8	+2.4	+2.6
15.0	4.0	8.0	15.0
+4.0	0.9	+1.0	+4.0
8.0	5.0	4.0	10.0
+4.4	+5.6	+0.7	+0.2
12.0	10.0	8.0	6.0
+1.8	+1.1		0.0
12.0	5.0		8.0
	+3.1		-0.3
	10.0		6
+4.0	+3.5	+1.0	0.0
10	5.0	1.0	8.0
+2.7	+0.5		+0.6
10.0	8.0		8.0
+2.7	16.3		+1.6
10.0	4		3.0
+3.2	+1.1		+0.4
10.0	8.0		6.6
	+2.4		-0.5
15.0	7.0		6.0
+0.8			-2.4
15.0			5.0
+0.5			-2.8
15.0			2.0

out of "118" lake

+1.4	-2.0	+0.6
8.0	5.0	12.0

99.73

Station	B.S. +	I.I. 33	F.S. -	Elevations
21 1+9			5.1	1101.2
+50			7.2	1099.1
12 ² 4			5.7	1100.6
12 ³ 7			6.9	1099.4
12 ⁴ 3			6.8	1099.5
7 Ext 12 ⁵ 5			8.1	1098.2
+30			6.1	1100.2
12 ⁶ 4			4.4	1101.9
+30			7.5	1099.8
12 ⁷ 5			8.1	1098.2
+25			6.9	1099.4
12 ⁸ 5			8.1	1098.2
+50			4.4	1101.9
T.P.			-6.57	1099.76
	+4.75	1104.51		
12 ⁹ 7			3.7	1100.9
+50			4.9	1099.6
130 128			6.0	1098.5
+20			7.0	1097.5

water 0.2 deep riffle

" 1.4 deep

water 0.6 deep

Left \$ Right

+0.7	+0.6	-1.6	+6.0
12.0	8	12.0	
	+1.3	+1.8	+3.1
	10.	8.0	10.0
-0.9	+0.3	+1.6	
12.0	5.0	3.4	10.0
+1.3	+1.1	+0.5	0-5
10.	6.0	10.0	12.0
+2.5	0.0	+0.4	+1.7
5. X 12.	3.0	10.	12.0
+0.0.4	-0.4	+1.3	+4.0
15.0	10.0	9.0	12.0
+2.1	1.2	+1.1	
12.	10.00	15.	
-0.4		-0.1	
15.0	0	15.0	
+2.3	+1.1	+0.5	+0.4
12.	6.	5.0	12.
	+2.0	+0.6	+3.8
	12.00	8.0	10.7
+1.9+0.9	-0.9	+1.8	1.7
15.	10.	8	15.0
+2.2+3.9	+2.0	+1.0	+2.9
15.0	9.0	7.0	5.0
	-0.5	-1.0	-3.6
	10.7	15.0	4.0
			12.7
			15.

Top of rock 40' R of 126+75

+0.2	+0.7	-0.8
15.	6.0	15.
+1.0	+1.4	+0.1
15.	7.0	7.
	3.0	12.0
	-0.9	+0.3
15.7	2.0.	15.
		0.0
		10.

	BS+	AD	FS - Elevation
+25	1104.5 ⁵		3.9 1100.6
+75			4.0 1100.5
129			2.2 1102.3
+25			6.3 1098.2
+40		water 2. def	7.7 1097.1
+60			3.3 1101.2
+80			6.6 1097.9
130 ²			7.4 1097.1
+50			6.5 1098.0
137 ³			4.4 1100.1
+70			6.5 1098.0
137 ¹			7.4 1097.1
+25			6.7 1097.8
+65			5.8 1098.7
135 ⁵			7.7 1096.8
T.P.			2.13 1102.38
133 ⁵	1157	1103	9
+75			7.8 1096.1
134 ⁶			7.6 1096.3

5-
Right-29

Lt.			
	+0.3	0	0.0
	15.0	7.0	10.7 15.0
	-2.0	0.0	-1.3 -1.5
	18.0	15.0	10. 15.0
	-6.0	0.0	-0.2 -3.3 -4.2
	15.0	5.0	5.0 10. 15.0
	-0.7	+3.5	+1.8
	2.0	15.0	8.0 0
	10.0	18.0	+1.0 +3.5
	+3.7	+4.1	+2.0 +3.0
	15.0	9.0	5.0 0
	-0.7	8.0	8.0 12.0
	15.0	0	-0.2 -3.6 -4.2
	+0.5	-0.7	+1.4 +2.8
	15.0	6.0	7 12.0
	+2.2	+3.9	+0.3 +3.2 +3.8
	15.0	10.0	3.0 4.0 10.0
	+2.1	+2.0	-0.4 +0.8
	10.0	4.0	5. 15.0
	-0.4	0.0	15.0
	15.0	0	15.0
	+2.0	+1.6	-2.0 -2.0 +0.2 +0.9
	15.0	8.0	6.0 6.0 7. 15.0
	+2.0	-0.6	-0.5 +0.2
	15.0	11.0	5.0 4.0
	+2.9	+1.0	0.0 +2.0
	15.0	1.0	6.0 15.0
	+2.5	+2.0	-1.7 -0.7
	15.0	5.0	5.0 15.0
	+2.5	+2.0	0.0 -1.4 -3.0
	15.0	5.0	6. 10. 15.0
	+3.6	+1.3	-0.6 +0.5 +3.6
	18.0	15.0	6.0 10.0 12.0
baseline root 25L of 133 +25			
	+3.7	+3.5	-0.5 +0.2
	15.0	2.0	5.0 15.0
	+3.5	+2.7	-0.2 -0.4 +3.0
	15.0	7.0	5.0 12.0 15.0

Station	H.S.	FS - Elevations
13 ⁶	+B.S. 1103.92	
+75		7.1 1096.8
Ext. 7'		
13 ⁵⁻⁷		6.3 1097.6
+40		6.7 1097.2
13 ⁶	water 1.3 deep	8.9 1095.0
+25		7.8 1096.1
+85		6.8 1097.1
13 ⁷		5.0 1098.9
+50	water 1.6 deep	9.2 1094.7
140		
138		7.9 1096.0
+50		8.0 1095.9
141		
139		5.5 1097.4
+25	water 1.3	10.0 1093.9
+25	to Navvoo Ditch	9.2 1094.7
100 ft up "	water 1.2 deep	9.1 1094.8
+50		8.5 1095.4
Ext 8'		
140 ²		7.8 1096.1
141 ³	1.6 deep	10.4 1098.5
T.P.	see Hammer	7.21 1099.71

as checked by F.K.

Left	Right
+2.5	+1.6
3.0	5.1
+1.5	+1.6
15.0	3.0
-0.9	-1.1
15.0	12.00
+4.5	+4.1
15.0	10.0
	+1.4
	15.0
0.0	+1.1
15.0	5.0
-1.3	-1.7
18	12
	+3.4
	15
	+1.1
	15
	+2.7
	15
	-2.2
	16
+1.4	+2.0
15.0	10
	+0.8
	7.00
	10.0
-0.2	-1.7
18.0	10.00
+0.8	-2.0
15.0	8
	+3.3
	8
	+1.4
	5.0
	3.0
	5.0
	10.0
	15.0
	+2.1
	8.0
	+1.2
	18.00
	0.0
	+2.7
	5.0
	+3.4
	10.0
	15.0

Bent 20" spike in NW corner 14" maple to left of old

Sat, P.M. Fuel & Diet 6.90
 1,093.08

Sta	B.S.†	H.D. 200	F.S. - Elev.
147 ³ 6.35	+2.27	1101.98	1099.71
+30		water = 1.6 deep	8.4 1093.6
+85			5.1 1096.9
148 ⁴			6.4 1095.6
+60			7.7 1094.3
6.615 148.5		water 1.2 deep	8.2 1093.8
+75			7.0 1095.0
144 ^c			4.8 1097.2
+15			7.2 1094.8
+50		water 1.0 deep	8.2 1093.8
148 ⁷			7.2 1094.8
+20			7.0 1095.0
+50			4.4 1097.6
146 ⁸			4.9 1097.1
+40			7.7 1091.3
+85 in drive to Sugarhouse			7.5 1094.5
147 ⁹			4.5 1097.5
+30			5.0 1097.0
+50			8.2 1093.8

Left: ♀ Right

boat wire spike 60' R of 1+1

+4.0	+3.4	+1.6	-1.4	+2.4	+4.0
15.0	10.0	5.0	3.0	5.0	15.0
	0.0	-0.3	+0.2		+0.3
15.7	10.0	5.0	5.0		15.0
-1.2	-0.9	-0.6	+1.0		+1.7
15.0	10.0	5.0	5.0		15.0
+3.7	+2.2	+0.7	+0.7	+2.3	+2.8
15.0	10.0	3.0	5.0	10.0	15.0
+3.4	+2.4	+1.2	+1.3	+3.5	+4.0
15.0	10.0	5.0	5.0	8.0	15.0
	+2.7	+2.3	-0.7		0.0
	15.0	5.0	10.0		15.0
	+0.3	-0.4	-2.2	-4.2	-4.0
	15.0	10.0	3.0	4.0	15.0
+2.7	+1.9	+2.8	-3.0	-2.4	
10.0	10.0	5.0	1.0	15.0	
	+3.2	+1.0	+0.9	+4.0	
	15.0	10.0	8.0	15.0	
+2.3	+0.3	-1.8	+1.0	+1.4	
15.0	10.0	8.0	5.0	15.0	
	+2.3	+2.0	-2.0		0.0
	15.0	2.0	2.0		15.0
	-1.0	-1.2	-0.5	-0.2	
	15.0	6.0	5.0	10.0	
		0.0	-0.6	-3.4	-4.0
		5' x 15'	4.0	7.0	10 x 2.0
+1.9	+2.0	0.0	-1.0	-1.3	
10 x 15'	9	6.0	5.0	10 x 15'	
	-1.3	-1.0	+3.0	+2.0	
	10 x 15'	3.0	5.0	15.0	
	-4.0	-2.2	0.0		
10.7 15'		5.0	10.0 x 15'		
-3.0		-2.5	0.0		
15.7 10'		2.0	10.0 x 15'		
+1.4	+0.5		+0.5	+3.4	+3.0
15.0	10.0		5.0	8.0	10.7 15'

27

F.S. - Elev.

2.8 1099.2

9.5 1092.5

water 1.2 dup

8.9 1093.1

-4.86 1097.12

+2.66 1099⁸⁰ 78

+20

7.6 1092.2

+25

3.0 1096.8

water 1.5 dup

15²

7.0 1092.8

water about 3.00 dup

15³

8.0 1091.8

+16 = 28+0

+06

1.2 1098.6

15⁴

8.6 1091.2

64 + 1.0

+30

5.26 1094.2

15⁵

5.1 1094.7

15⁶

8.1 1091.7

15⁷

5.5 1094.3

water for nipples

15⁸

6.6 1093.2

water 0.1

15⁹

6.9 1092.9

water 0.3

2¹ ext

+52

7.0 1092.8

+75

✓ 4.9 1094.9

Left:

Rt.

25-

apparent high water mark

+4.3	+3.0	-0.3	+4.0	+3.5
15	12	10	6.0 x 10	15
+3.6	+1.2		0.0	
15.0	10.0		15.0	

west root of 80° ash ^{on} bent nail

+4.5	+3.5	0.0	0.0	
10 x 15	7	5.0	5.0 x 15	
+0.6	+0.2		-4.5	-3.5
15.0	10.0		5.0	15.0
+3.5	+1.5		+1.2	+3.5
15.0	10.0		6.0	10.0
on Ry	+5.0	+2.5	-0.2	0.0
	15.0	8.0	5.0	15.0 x 20.0

Top of 8.40 Ry road bed. L side

+3.0	+5.25	0.0	0.0	+1.0
9.0	12.0	0	5.0	15.0
+1.3	+1.4		-1.4	-2.0
15.0	8.0	0	5.0	10.0
+1.1	+1.0	+1.0	-1.5	-2.0
15.0	5.0	10.0	6.0	10.0 x 15.0
+3.3	+3.5	0.0	0.0	
10 x 15	8	6.0	5.0 x 15	
+2.2	+0.8		-0.5	0.0
15.0	12.0	10.0	5.0	10.0
+2.6	+2.4	+0.5	0.0	+1.5
15.0	12.0	1.0	7.0	10.0 x 15.0
+2.5	+0.9	-0.3	-0.4	+1.7
15.0	12.0	7.0	5.0	10.0
+2.5		7.0	-0.5	
10 x 15.0		5.0	5.0 x 15.0	
0.0			-1.5	-3.5
5.0	15.0	0	10.0	15.0 x 20.0

	BS+	H ₂ O	♀	♂	F.S. - Evers
16 ⁷					
+92					1098.29
16 ⁸					7.6 1093.7
+40					4.7 1093.6
+50		water 0.0			5.4 1092.9
					6.7 1091.6
+70					8.2 1090.1
+75					5.1 1093.2
16 ⁹					4.7 1093.6

quit at 6:30 P.m. Big storm

Thursday Full moon Runway - April 15-16-1911
 (T. P. above) +5.09 1098.62

16 ⁹ +50					5.20 1093.4
+65-		water 0.0			7.18 1091.44
170 16 ⁸					7.18 1091.44
+10					5.1 1093.5
+20					5.8 1092.8
+60					5.1 1093.5
+70					7.2 1091.4
+90					7.2 1091.4
171 +69					6.0 1092.6
+20					7.2 1091.4

Left	♀	Right
same as ♀	0	same as ♀
" " "	0	" " "
" " "	0	" " "
" " "	0	" " "
" " "	0	" " "
" " "	0	" " "
" " "	0	" " "

8 root of big ash 167+20

-1.0	5.0	+0.3	-0.5	0.0
15.	10.	8.0	5.	-10. x 15.
-0.8		-0.5	+0.9	+1.0
10. x 15.		2.0	5.	10. x 15.
+2.4		+2.5	-0.8	
10. x 15.		4.0	10. x 20	
+0.9		+0.8	-1.0	-2.2
15.		10.	2.0	5.0
			+0.5	-0.1
			8	10
				15
			-0.7	-2.05
			3.0	6. x 20
+0.6	+0.5	-0.4	-0.5	1.1
15.	10	5.	5.	20.
-2.0		-1.3	+1.0	+1.9
10. x 2.0.		5.	5.	10. x 15.
-2.5		-1.2	+0.9	+0.18
10. x 15.		3.0	5.	10. x 15.
-1.4		-0.5	+1.2	+1.6
10. x 15.		5.0	5.0	10. x 15.

BS+	AD	FS - Elevs	
169 ⁷ +00	1098.62	5.8 8.2	1090.3
175 ²		5.5	1093.1
+25		6.9	1091.7
+60		water 0.0 7.55	1091.07
+70		5.8	1092.8
17 ³		6.9	1091.7
+10		water 0.4 8.0	1091.02
1 ang. 100			1090.6
+30		9.3	1089.3
+50		8.2	1090.4
+80		6.6	1092.6
17 ⁴		6.5	1092.1
+40		8.5	1090.1
+60		10.0	1088.62
T.P.		-1.02	1099.60
	+1.61		1099.21
+		1.5	1097.4
		2.5	1096.7
		4.2	1095.0
		5.3	1093.9

Left	±	Right
5. X 15	+3.0 3.0	0.0 + 0.5 2.0 10 X 15
	0.0 15	0.0 -1.7 10 15
-0.4 10 X 15	-0.3 4.0	-0.4 -1.0 5. 10 X 15
	-1.0 -0.6 10 X 20 5	+1.6 +1.9 5.0 10 X 15
-2.2 10 X 15	-1.7 6.0	0.0 15
-2.0 15	-1.0 -0.6 10.0 6	+0.2 +0.8 4.0 15
+1.6 15	-1.5 -1.3 10.1 2.5	+0.6 +1.0 +1.2 6. 10 15
+2.0 +2.4 +1.0 15 10 6	0	+1.2 +2.5 10 15
+1.6 15	+1.0 6	0
-2.4 10 X 20	-1.8 4.0	+1.1 +0.8 5.0 10 X 15
-2.8 -2.4 15 10	-1.6 8.0	-0.2 +0.9 9.0 11 X 15
-1.0 10 X 20	-0.6 5.0	+0.3 +1.4 +2.5 6 10 15 X 20
-0.6 20	0.0 10	+1.0 +2.0 +2.7 10 12 15 X 20
Primary U.S. Geol. Surv. B.M. 117 Parapet S.W. cor. bridge over Phelps creek		
floor of bridge at ± of creek + highway " seat at W. end ± road 25' W. of Wend Bridge " " 45' " " "		

Sto.	AD	FS - Elevation
BS+ 1099.21		3.8 1095.4
		1.9 1097.3
		3.6 1095.6
		5.0 1094.2
		4.6 1094.6
		3.0 1096.2
		(1102.0)
17 ⁵		11.0 1088.2
+75		10.5 1088.7
17 ⁶		10.6 1088.6
+30		8.8 1090.4
		-6.73 1092.48
+5.0	afterdin. came H.D.	7.7 1091.5
17 ⁷		7.5 1091.7
+60	water 0.6 det	1090.41
		9.4 1089.8
17 ⁸		8.3 1090.9
+25		9.9 1089.3
17 ⁹		10.2 1089.0
<u>1735</u>		8.56 1090.65
		-6.73 1092.48

4 cent of road
 200 ft. west of bridge near W apple trees
 300 " " "
 250 East " "
 85 " " "
 12.5 " " "

rise of about 6 ft in next 100 E.
 0.0 -0.5 +2.0 +2.5
 15. 10. 0 11. 15.
 +4.7 +4.0 +3.5 +1.8 +2.0 +3.7
 15. 13 8 6. 0 12. +15
 +4.8 +2.3 +2.0 +4.0
 15. 10 8 0 6.0 10 x 15.
 +2.5 +0.7 -0.1 +0.6 +2.0
 15. 0 10. 6. 0 6 8 x 15

Dinner peg 8 1/2 N. of blazed 6" Blm.
 -1.7 -1.3 +0.7
 15 8. 0 5. x 15.
 -2.7 -0.7 +0.6 0.0 +0.5
 15. 12. 6. 0 10. 15.
 0.0 +1.7 +1.5 +1.7
 10 x 15. 3. 7. 15.
 -1.7 -0.8 -0.5 -1.0 -2.0
 15. 6. 2. 4. 6. 10. 15.
 -0.6 +1.2 +1.3 +0.3 +0.2 +0.6
 11 x 15 16 7 8 10 12 x 15
 +2.1 +2.0 0.0 0 pane as E for 20.
 10 4 3. surface of water

Sta	B8+	H.D.	-FS	Flc5
	+5.65	1098	13	1092.48
⁹ 178+50				8.6 1089.5
² 12'L 178/80				9.0 1089.1
¹⁸¹ 179				9.1 1089.0
² 180				9.2 1088.9
+40				6.0 ⁹ 1082.1
+50				7.80 1090.33
187 ³				6.0 1092.1
+35				6.6 1091.5
TP				-5.88 ⁵ 1092.25
+40	+2.73	⁹⁵ 1094.98		4.9 1090.1
+50				4.5 1090.5
+60				5.3 1089.7
+70				4.1 1090.9
188 ⁴				3.7 1091.3
+3.0				4.0 1091.0
+40				6.1 1088.9
+60				6.0 1089.0
183 ⁵				7.2 1087.8

water 0.4

Left \$ Right

same as \$	0	same as \$	1
+2.4	+0.9	+2.0	+3
15	12	10	15
+2.1+2.3+1.2	0.0	-0.5	
15	11	7	5
+3.2+1.3	+1.5		
20	15	10	0
same as \$	0	5.0	7.0
		-1.8	-3.8

water surface same as ^{on} February

same as \$ 0 at \$ 15R+L
" " " 0 " " " " "

Reg 15'L of 181+35

average with \$	0	average with \$ 15R+L	
-	-	-	-
-	-	-	-
-	-	-	-
-	-	-	-
-	-	-	-
-	-	-	-
-	-	-	-
-	-	-	-
+1.0	0.0	+1.3	+3.7
15	10	5	7
		+4.0	
		15	

1091 34

Me	BST	H J	T.S -	Elev
18 ⁵ +10		⁹⁵ 98	3.8	1091.2
+20			4.6	1090.4
15 ⁶			5.0	1090.0
+70			4.9	1090.1
+75			5.8	1089.2
18 ⁷		water	1.0 deep	1088.9
+50			7.1	1087.9
+85			7.4	1087.6
15 ⁸			6.1	1088.9
18 ⁹			4.7	1090.3
+50			6.2	1088.8
+50			6.73	1088.25
+50			8.5	1086.5
T.P.			-4.92	1090.06
	⁸⁰ +4.81	⁹⁶ 1094.84	18 ¹⁰ deep	1088.3
190		water	8.4	1086.5
+50			6.6	1088.3
+75			4.6	1090.3
191			5.1	1089.5
+10			✓ 7.1	1087.8

Left $\frac{1.8}{2}$ Right

15' average with $\frac{1.8}{2}$	0	average with $\frac{1.8}{2}$ for 15'		
15' " " " " " "	0	" " " " " "		
" " " " " "	0	" " " " " "		
" " " " " "	0	" " " " " "		
" " " " " "	0	" " " " " "		
$\frac{+0.6}{15}$	$\frac{0.0}{10}$	$\frac{+0.3}{7}$	$\frac{+2.7}{9}$	$\frac{+3.9}{15}$
same as $\frac{1.8}{2}$	0	same as $\frac{1.8}{2}$	15' R+L	
$\frac{+2.0}{15}$	$\frac{+1.3}{10}$	0	" " " "	20' R
$\frac{+0.3}{15}$		0	$\frac{-1.4}{8}$	$\frac{-1.9}{15}$
$\frac{+0.2}{15}$	$\frac{-0.3}{10}$	0	$\frac{0.0}{2}$	$\frac{-1.7}{3}$
		0	$\frac{-1.6}{10}$	$\frac{0.0}{15}$
water surface				
$\frac{+0.7}{10 \times 15}$	$\frac{+0.3}{5}$	0	$\frac{+0.6}{5}$	$\frac{+1.2}{10}$
			$\frac{+1.6}{15}$	
Top of Ref. stake = 188				
$\frac{+3.0}{15}$	$\frac{+2.5}{10}$	$\frac{+1.6}{8}$	0	$\frac{0.0}{5}$
				$\frac{+1.0}{15}$
$\frac{+2.0}{15}$	$\frac{+2.2}{5}$	$\frac{+1.8}{2}$	0	$\frac{-2.0}{5}$
				$\frac{-1.2}{10}$
				$\frac{0.5}{15}$
average with $\frac{1.8}{2}$ 15'	0	0.0	with $\frac{1.8}{2}$ 15'	
" " " " " "	0	-	" " " " " "	
" " " " " "	0	-	" " " " " "	

192 ¹			
+90	1092 92	5.0	1087.9
193 ⁵		5.7	1087.2
+35		5.1	1087.8
+80		7.1	1085.8
+95		5.7	1087.2
194 ⁶		4.4	1088.5
ang. 100 tang.		5.0	1087.9
+90		5.7	1087.2
194 ⁷	water 0.3 def.	7.3	1085.6
194 ⁸		5.8	1087.1
+15		7.00	1085.92
B.M.		-3.41	1089.51

5-8
1.5
7.3

5-5-5

same as 2 for 15 ft. R + L of 2

" " " 15 L 0

$$\begin{array}{r} +1.0 \\ 5- \\ \hline \end{array} \quad \begin{array}{r} +3.4 \\ 10 \\ \hline \end{array} \quad \begin{array}{r} +3.5 \\ 15 \\ \hline \end{array}$$

$$\begin{array}{r} -0.7 \\ 15 \\ \hline \end{array} \quad \begin{array}{r} -0.8 \\ 6.0 \\ \hline \end{array} \quad \begin{array}{r} +0.5 \\ 5.0 \\ \hline \end{array} \quad \begin{array}{r} +2.0 \\ 10 \\ \hline \end{array} \quad \begin{array}{r} +2.0 \\ 15 \\ \hline \end{array}$$

$$\begin{array}{r} +0.6 \\ 15 \\ \hline \end{array} \quad \begin{array}{r} +1.0 \\ 10 \\ \hline \end{array} \quad \begin{array}{r} +0.6 \\ 10 \\ \hline \end{array} \quad \begin{array}{r} +1.0 \\ 12 \\ \hline \end{array} \quad \begin{array}{r} +2.3 \\ 15 \\ \hline \end{array}$$

$$\begin{array}{r} +3.0 \\ 15 \\ \hline \end{array} \quad \begin{array}{r} -1.3 \\ 15 \\ \hline \end{array}$$

+1.9 15. Same as 2 for 15-

same as 2 for 15" R + L of E

" " " " " " " "

" " " " " " " "

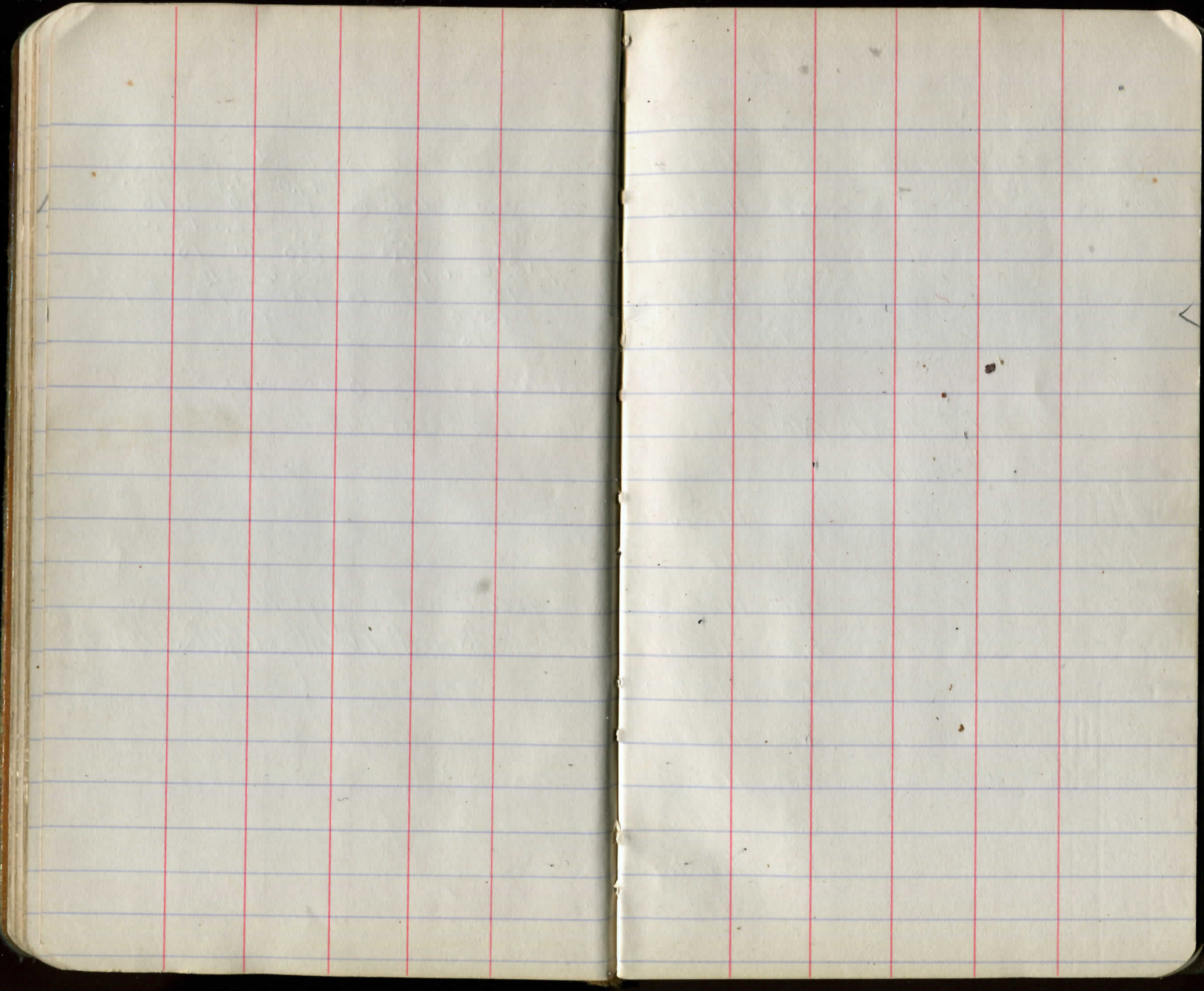
" " " " " " " "

15 198 approx

surface of water large pond & open channel

nail in S. post. 16" Maple to R. of 194+90

22.3'



Hanna. 10/12/15
Mintern LATERAL No 1

Sta.	B.S.	H.T.	F.S.	Elev.
B.M.	6.39	11.31.17		1124.78
0			3.9	1127.3
1			5.2	1126.0
2			5.7	1125.5
3			6.7	1124.5
+12.6			6.7	1124.5

LATERAL No 2

1131.17

0			2.3	1128.9
1			1.9	1129.3
+20			2.4	1128.8
2			2.2	1129.0
3			3.3	1127.9
4			4.2	1126.0
5			5.8	1125.4
6			6.2	1125.0
+25			6.7	1124.5

Fair Warm

On maple across road from King's house

± 3' to Lt. of transit line.

Drive way

Sta	B.S.	H.I.	F.S.	Elev.
7		1131.17	6.3	1124.9
8			6.7	1124.5
+85			7.3	1123.9
9			7.0	1124.2
+60			8.2	1123.0
10			8.6	1122.6
11			9.8	1121.4
+16.3			10.0	1121.2

MAIN LINE

B.M. 4.10	1124.16		1120.06
43		4.7	1119.5
44		5.9	1118.3
45		6.2	1118.0
46		7.0	1117.2
47		6.2	1118.0
48		6.8	1117.4
+50		5.1	1119.7
49		7.3	1116.9

stakes
15' to
Lt. of \mathcal{L}

\mathcal{L}

0.0
0.0

0.0
0.0

0.0
0.0

0.0
0.0

0.0
0.0

-1.7
15

0.0
15

+0.1
15

+0.3
15

+0.4
15

0.0
15

-0.3
15

-0.5
15

-1.7
30

0.0
30

+0.4
30

+0.9
30

+0.4
30

+0.1
30

-2.4
30

-0.7
30

Sta.	B.S.	H.I.	F.S.
50	1124 10	6.2	1118.0
+46.5		6.8	1117.4
B.M.		5.88	1118.28

$$\frac{+0.2}{1.5}$$

$$\frac{-0.5}{3.0}$$

$$\frac{-0.3}{1.5}$$

$$\frac{-0.2}{3.0}$$

Notch in Hickory about 50'S. of sta 48+50

stakes 15'
E. of E

LATERAL No 3

B.M.	3.93	1122.21		1118.28
------	------	---------	--	---------

21		5.0	1117.2
----	--	-----	--------

20		4.7	1117.5
----	--	-----	--------

+55		5.8	1116.4
-----	--	-----	--------

19		4.9	1117.3
----	--	-----	--------

18		4.4	1117.8
----	--	-----	--------

17		4.0	1118.2
----	--	-----	--------

16		3.9	1118.3
----	--	-----	--------

15		3.5	1118.7
----	--	-----	--------

14		3.2	1119.0
----	--	-----	--------

T.P.	3.79	1125.02	0.98	1121.23
------	------	---------	------	---------

13+8.8		5.6	1119.4
--------	--	-----	--------

12		6.1	1118.9
----	--	-----	--------

$$\frac{-0.2}{1.5}$$

level

$$\frac{-0.2}{1.5}$$

$$\frac{-0.8}{2.5}$$

$$\frac{0.0}{1.5}$$

$$\frac{-0.3}{1.5}$$

$$\frac{-0.9}{2.8}$$

$$\frac{-0.4}{1.5}$$

level

$$\frac{-0.6}{1.5}$$

$$\frac{-0.1}{2.5}$$

$$\frac{-0.3}{1.5}$$

$$\frac{-0.8}{2.5}$$

$$0.0$$

$$\frac{+0.4}{2.8}$$

$$\frac{-1.4}{3.0}$$

$$\frac{0.0}{0.0}$$

$$\frac{0.9}{7}$$

$$\frac{-1.6}{10}$$

$$\frac{-0.6}{1.5}$$

$$\frac{-0.4}{2.0}$$

$$\frac{0.0}{0.0}$$

$$\frac{-0.4}{7}$$

$$\frac{-1.4}{1.5}$$

$$\frac{+0.2}{2.5}$$

$$\frac{0.0}{0.0}$$

$$\frac{+1.0}{1.5}$$

$$\frac{+0.1}{1.7}$$

$$\frac{+0.9}{2.5}$$

Sta.	B.S.	H.I.	F.S.	Elev.	
B.M.	1125.02	4.25	1120.77		on S. side of 2' Elm S. of road.
11		4.8	1120.2		$\frac{-0.9}{1.4} \frac{-1.2}{1.5} \frac{0.0}{1.8} \frac{-0.5}{2.5}$
10		4.5	1120.5		$\frac{+0.3}{1.0} \frac{-1.2}{1.3} \frac{+0.1}{1.5}$ - level
9		3.9	1121.1		$\frac{0.0}{0.0} \frac{-0.3}{6} \frac{-1.3}{10} \frac{-0.4}{1.5}$ Level
8		4.8	1120.2		$\frac{0.0}{0.0} \frac{+0.6}{1.5}$ Level
7		4.0	1121.0		$\frac{0.0}{0.0} \frac{-0.4}{1.5}$ Level
6		3.1	1121.9		$\frac{-0.8}{3} \frac{-1.3}{1.5} \frac{-0.4}{2.5}$
B.M.	5.30	1128.14	2.18	1122.84	Nitch in root of 20" oak 50' E of Sta. 6
5		5.3	1122.8		$\frac{-1.0}{1.5} \frac{-1.0}{2.5}$
4		4.7	1123.7		$\frac{0.0}{0.0} \frac{-0.4}{1.2} \frac{-1.5}{1.5} \frac{-1.6}{2.5}$
3		5.6	1122.5		$\frac{0.0}{1.5}$
+50		3.7	1124.4		0.0
2		5.3	1122.8		0.0
1		5.0	1123.1		0.0
0		3.8	1124.3		0.0

MAIN LINE

Warm
Springlike

Sta. B.S. H.T. F.S. Elev.

B.M. 5.22 1123.50 1118.28

51 6.1 1117.4

52 6.1 1117.4

T.P. 1.89 1120.77 4.62 1118.88

53 4.3 1116.5

54 4.8 1116.0

55 6.1 1114.8

+50 5.9 1114.9

+52 4.2 1116.6

56 4.4 1116.4

B.M. 3.19 1120.48 3.48 1117.29

57 5.0 1115.5

+60 5.8 1114.7

+65 4.3 1116.2

58 4.9 1115.6

59 4.7 1115.8

60 6.0 1114.5

Hickory near 48+50

$\frac{0.0}{0.0}$ $\frac{-0.1}{15}$ $\frac{-0.8}{20}$ $\frac{-1.4}{22}$ $\frac{-1.4}{30}$

$\frac{0.0}{0.0}$ $\frac{0.0}{7}$ $\frac{-0.9}{10}$ $\frac{-0.9}{15}$ level

$\frac{0.0}{0.0}$ $\frac{-0.6}{15}$ level

$\frac{0.0}{0.0}$ $\frac{+0.6}{10}$ $\frac{-1.4}{14}$ $\frac{-1.4}{15}$ level

$\frac{0.0}{0.0}$ $\frac{+0.2}{15}$ $\frac{+0.2}{25}$

00

00

Level

On W. side 2' Oak 25' to Pt. of 55+90

$\frac{+0.5}{15}$ $\frac{+0.5}{30}$

00

00

$\frac{-0.2}{15}$ $\frac{+0.3}{25}$

$\frac{-0.7}{15}$ level

$\frac{+0.4}{15}$ level

Sta. B.S. H.I. F.S. Elev.

T.P. 3.40 1119 04 4.84 1115.64

61 4.2 1114.8 $\frac{0.0}{0.0}$ $\frac{+0.4}{15}$ level

62 5.0 1114.0 $\frac{0.0}{0.0}$ $\frac{+0.1}{15}$ level

B.M. 3.74 1115.30

63 5.2 1113.8 $\frac{0.0}{0.0}$ $\frac{-2.1}{3}$ $\frac{-0.3}{6}$ $\frac{-0.2}{15}$ and 25

64 6.9 1112.1 $\frac{0.0}{0.0}$ $\frac{-1.5}{7}$ $\frac{-0.3}{9}$ $\frac{+1.4}{15}$ and 25

T.P. 3.33 1118 42 3.95 1115.09

65 7.0 1111.4 $\frac{0.0}{0.0}$ $\frac{+0.7}{7}$ $\frac{+2.2}{15}$ same 25

66 5.0 1113.4 $\frac{0.0}{0.0}$ $\frac{0.0}{6}$ $\frac{-2.1}{8}$ $\frac{-2.2}{12}$ $\frac{-0.6}{15}$ same 25

67 6.9 1111.5 $\frac{0.0}{0.0}$ $\frac{-0.6}{13}$ $\frac{+1.6}{15}$ $\frac{+0.4}{25}$

+25 7.5 1110.9 $\frac{0.0}{0.0}$ $\frac{0.0}{15}$

68 7.0 1111.4 $\frac{0.0}{0.0}$ $\frac{-0.1}{15}$ level

T.P. 4.10 1117 27 5.25 1113.17

69 5.1 1112.2 $\frac{0.0}{0.0}$ $\frac{-0.2}{15}$ level

70 4.4 1112.9 $\frac{0.0}{0.0}$ $\frac{+0.2}{15}$ $\frac{-0.5}{25}$

+60 5.9 1111.4 $\frac{0.0}{0.0}$ 00

+65 7.3 1110.0 $\frac{0.0}{0.0}$ 00

Or. big Elm W. of Sta 62

Sta. B.S. H.T. F.S. Elev.

71	1117.27	7.9	1109.4
72		6.2	1111.1
TP	6.30 1116.82	6.75	1110.52
73		7.0	1109.8
74		7.0	1109.8
+70		7.1	1109.7
+85		5.4	1111.4
75		7.5	1109.3
+15		6.7	1110.1
+35		7.5	1109.3
+50		4.9	1111.9
76		5.1	1111.7
77		7.0	1109.8
T.P.	4.91 1116.19	5.54	1111.28
B.M.		4.40	1111.79
+55		6.9	1109.3
+57		5.1	1111.1

15'
offset

±

$\frac{0.0}{0.0}$	$\frac{0.0}{1.5}$	$\frac{+0.3}{2.5}$
$\frac{0.0}{0.0}$	$\frac{+1.0}{1.5}$	SAME 25
$\frac{0.0}{0.0}$	$\frac{+0.5}{1.5}$	$\frac{+0.5}{2.5}$
	$\frac{+1.4}{1.5}$	$\frac{+1.5}{2.5}$
	$\frac{0.0}{0.0}$	
	$\frac{0.0}{0.0}$	
$\frac{0.0}{0.0}$	$\frac{+0.8}{1.0}$	$\frac{+2.1}{1.5}$
	$\frac{0.0}{0.0}$	$\frac{2.0}{2.5}$
	$\frac{0.0}{0.0}$	
	$\frac{0.0}{0.0}$	
$\frac{0.0}{0.0}$	$\frac{-0.2}{1.5}$	$\frac{-2.2}{3.0}$
	level	
	Hickory W. of Sta. 78	
$\frac{0.0}{0.0}$	$\frac{0.0}{0.0}$	$\frac{0.0}{0.0}$
$\frac{0.0}{0.0}$	$\frac{0.0}{1.5}$	$\frac{-1.5}{1.8}$
		$\frac{-1.5}{2.5}$

Sta B.S. H.I. F.S. Elev.

78	1116.19		
+85		5.5	1110.7
+90		6.8	1109.4
78		7.1	1109.1
T.P.	4.71	1115.85	5.05 1111.14
+50		5.9	1110.0
+80		7.0	1108.9
79		5.8	1110.1
+50		5.0	1110.9
+75		9.0	1106.9
80		5.5	1110.4
+15		5.3	1110.6
+50		6.4	1109.5
+70		7.0	1108.9
+80		7.9	1108.0
81		8.6	1107.3
+55		8.7	1107.2
+65		5.9	1110.0

00

Level

00
20

+0.2
15

+0.2
25

00
00

+0.3
15

+0.3
25

00
00

-1.5
10

-2.2
15

-2.9
25

-2.5
30

00

00
00

-1.9
7

-2.2
15

-2.2
30

00
15

Level

00
15

00
15

00
00

-0.4
15

+0.8
25

00

00

Sta. B.S. H.I. F.S. Elev.

82 1115 85 5.7 1110.2

T.P. 3.69 1114.41 5.13 1110.72

+25 4.5 1109.9

83 6.7 1107.7

+30 5.0 1109.4

+85 7.5 1106.9

84 5.6 1108.8

85 5.4 1109.0

T.P. 4.22 1114.03 4.60 1109.81

86 4.5 1109.5

87 7.6 1106.4

+20 7.5 1106.5

+30 5.3 1108.7

T.P. 4.42 1114.63 3.82 1110.21

88 5.2 1109.4

89 6.7 1107.9

90 5.4 1109.2

$\frac{00}{00}$

$\frac{00}{15}$

$\frac{-0.4}{25}$

Hub. 81+80

$\frac{00}{00}$

$\frac{-06}{12}$

$\frac{-2.0}{15}$

$\frac{-1.8}{30}$

$\frac{00}{00}$

$\frac{+0.3}{15}$

$\frac{+1.8}{25}$

$\frac{00}{15}$

$\frac{00}{15}$

$\frac{00}{00}$

$\frac{-1.9}{15}$

$\frac{-2.0}{25}$

$\frac{00}{00}$

$\frac{+0.2}{15}$

$\frac{-1.0}{25}$

$\frac{00}{00}$

$\frac{-0.1}{15}$

$\frac{-0.3}{25}$

$\frac{00}{00}$

$\frac{+0.1}{15}$

SAME

00

00

$\frac{00}{00}$

$\frac{-0.7}{15}$

$\frac{-1.8}{25}$

$\frac{00}{00}$

$\frac{+1.2}{15}$

$\frac{+0.9}{25}$

$\frac{00}{00}$

$\frac{-0.4}{15}$

$\frac{-0.9}{25}$

Sta. B.S. H. I. F.S. Elev.

91 1114 63 5.9 1108.7

92 6.4 1108.2

T.P. 7.62 1117 13 5.12 1109.51

+27.7 8.4 1108.7

93 4.8 1112.3

+50 4.4 1112.7

94 4.6 1112.5

95 5.7 1111.4

96 7.3 1109.8

97 10.8 1106.3

T.P. 4.07 1111 12 10.08 1107.05

+60 8.6 1102.5

+75 9.0 1102.1

B.M. 563 3.07 1108.05

$\frac{00}{20}$

$\frac{00}{00}$

00

$\frac{00}{00}$

00

00

$\frac{00}{15}$

$\frac{-0.1}{15}$

$\frac{00}{15}$

$\frac{+0.1}{15}$

00

$\frac{00}{15}$

$\frac{+0.1}{15}$

$\frac{-0.3}{15}$

$\frac{0.0}{15}$

$\frac{00}{15}$

$\frac{00}{15}$

$\frac{00}{30}$

level

$\frac{-0.1}{25}$

$\frac{-0.1}{30}$

$\frac{-0.5}{30}$

$\frac{0.0}{30}$

$\frac{-0.2}{30}$

$\frac{+0.1}{30}$

B.M. on Hickory to Ft. in Miller's lot.

LATERAL No 4

Sta. B.S. H.I. F.S. Elev.

B.M. 5.68 1113.73 1108.05

4 9.8 1103.9

3 7.7 1106.0

2 7.5 1106.2

1 6.6 1107.1

0+20 9.9 1103.8

0 8.8 1104.9

4.20 1109.53

B.M. 2.75 1110.50 4.75 1108.05

T.P. 7.35 1111.95 4.75 1107.60

B.M. 3.90 1111.95 1108.05

(Readings taken on ϕ - 15' to Lt. of stakes)

On Hickory root in P. Miller's lot.

2.5	8.2
6.7	6.8
<hr/>	<hr/>
1.8	1.4
	1.0
	<hr/>
2.2	2.9
8.8	7.2
4.6	6.5
<hr/>	<hr/>
10.5	1.7
7.9	9.2
4.5	4.3
<hr/>	<hr/>
5.4	3.9
1.1	
<hr/>	
4.9	

On N.W. stone of abutment of bridge

On Hickory root in P. Miller's lot.

110610	110805
4.35	2.45
<hr/>	<hr/>
111045	H.I. 1110.50
	Sta 4 1102.30
	8.20
	1110.50
	1102.00
Sta 1 1111.95	Sta 7+95 8.50
1103.20	1110.50
8.75	1102.6
<hr/>	Sta 3 7.90
1111.95	H.I. 1110.50
1103.5	0.2.9
8.45	Sta 2 7.60
<hr/>	H.I. 1110.50
1110.50	Sta 1 1107.30
4.50	1110.50
<hr/>	
1107.50	
4.25	
<hr/>	
1111.95	

10/16/15

Hanna
Mintern

cloudy
cool

(water high
average about 1')

Sta.	B.S.	H. I.	F.S.	Elev.
B.M.	3.47	1111	52	1103.25
98			9.3	1102.2
+65			6.4	1105.1
+72			7.6	1103.9
+80			6.7	1104.8
99			6.8	1104.7
+50			8.1	1103.4
100			7.0	1104.5
+75			7.5	1104.0
+80			5.8	1105.7
101			7.4	1104.1
102			8.4	1103.1
103			10.0	1101.5
104			10.5	1101.2
T.P.	4.82	1109	50	6.84 1104.68
+18			5.8	1103.7
+20			6.7	1102.7

History in Miller's			1st
00	1.5	$\frac{+3.1}{15}$	$\frac{+3.2}{25}$
00	5	$\frac{00}{15}$	$\frac{00}{25}$
		00	
		00	
		00	
		$\frac{+0.1}{15}$	$\frac{+0.2}{30}$
		$\frac{00}{15}$	$\frac{00}{30}$
		$\frac{+0.5}{15}$	$\frac{00}{30}$
		00	
		00	
		00	
		$\frac{+2.2}{15}$	level
		$\frac{+2.1}{15}$	$\frac{+2.7}{30}$
		$\frac{+2.8}{15}$	$\frac{+2.8}{30}$
		$\frac{+3.0}{15}$	$\frac{+3.3}{30}$
		00	
		00	
		00	

Sta.	B.S.	H.I.	F.S.	Elev.
105		1109.50	6.2	1103.3
106			5.9	1103.6
107			6.3	1103.2
108			5.6	1103.9
109			5.2	1104.3
110			5.8	1103.7
				1100.90
+377			6.5	1103.0
B.M.	343	1107.71	5.22	1104.28
+60			6.7	1101.0
+65			5.4	1102.3
111			4.5	1103.2
+75			5.8	1101.9
+80			7.0	1100.7
112			4.9	1102.8
113			7.5	1100.2
+05			5.1	1102.6
114			6.7	1101.0

00	0.9	-1.2	-0.8	+1.6		
00	5	7	15	25		
00	0.1	-1.6	-2.4	-1.5	-0.6	-0.6
00	5	7	15	20	30	
00	0.0	-1.9	-2.0	-0.3	+0.3	
00	5	7	15	20	30	
00		-2.8		-2.2	-1.5	
00		7	15	25	30	
00	0.0	-2.6	-3.0	-2.7	-1.0	-1.5
00	5	7	15	22	25	30
00	0.0	-1.9	-3.8	-3.8	-0.8	
00	8	10	15	25	30	
00	-1.3	-3.0	-1.0	+0.9		
00	3	12	15	25	30	
On derrick about 50' W. of Sta. 110						
				00		
				00		
				-1.0	-2.4	-2.9
				15	25	30
				00		
				0.0		
				-0.5	-2.3	-1.9
				5	7	15
				00		
				-1.0	-2.3	-0.5
				5	7	15
				00		
				+0.8	+2.3	+2.0
				15	20	25
				00		
				+0.1	+1.1	+1.7
				7	10	15
				00		
				+1.6	+1.6	
				25	30	

Sta. B.S. H. T. F.S. Elev.

115 1107.71 8.6 1099.1

T.P. 492 1107.37 5.26 1102.45

+15 5.2 1102.2

+20 6.5 1100.9

+40 8.7 1099.0

+60 7.5 1099.9

+65 5.5 1101.3

116 4.6 1102.8

117 5.5 1101.9

+50 7.0 1100.4

+55 6.0 1101.4

118 5.0 1102.4

B.M. 3.04 1105.52 4.89 1102.48

119 5.4 1100.1

+45 5.7 1099.8

+50 7.5 1098.0

+55 5.8 1099.7

$\frac{00}{99} \quad \frac{+0.7}{7} \quad \frac{+2.4}{10} \quad \frac{+2.9}{15} \quad \frac{+2.6}{30}$

00

00

00

00

00

$\frac{00}{10} \quad \frac{-0.9}{10} \quad \frac{-0.8}{15} \quad \frac{-3.1}{18} \quad \frac{-3.4}{25} \quad \frac{-3.0}{30}$

$\frac{00}{10} \quad \frac{-1.9}{15} \quad \frac{-3.2}{20} \quad \frac{+1.2}{25} \quad \frac{+0.2}{30}$

$\frac{00}{10} \quad \frac{-2.0}{10} \quad \frac{-1.8}{15} \quad \frac{+1.0}{20} \quad \frac{+1.0}{30}$

00

$\frac{00}{10} \quad \frac{-0.2}{15} \quad \frac{+0.1}{30}$

On W. root E. Elm 75' E Sta. 110+25

$\frac{00}{10} \quad \frac{+0.2}{15} \quad \frac{+0.4}{30}$

00

00

00

5+9 B.S. H. I. F.S. EICK

120 1105.52 5.5 1100.0

+60 7.1 1098.4

+67 4.4 1101.1

121 7.4 1098.1

122 5.9 1099.6

+40 3.2 1102.3

123 5.5 1100.0

T.P. 534 1105.73 5.13 1100.39

+50 6.5 1099.2

+55 6.2 1099.5

+75 8.3 1097.4

124 6.1 1099.6

125 6.3 1099.4

+40 6.7 1099.3

+60 4.9 1100.8

+65 7.8 1097.9

B.M. 4.00 1101.73

15'
offset
line

9

+0.1
15 -1.8 -2.5 +0.5
18 25 30

00

00

+0.9 +3.8 +3.0
7.10 15

+2.9
30

+0.4
5 +1.6
15

+1.7
30

00

-2.2
5 +1.4
10 +1.1
15

+1.6
30

0.0

2.0
5 -2.1
3 -1.0
15 -0.7 +0.4 +1.1
20 25 30

0.0

+1.2
5 +1.2
15

+0.8 -0.4
25 30

0.0 +0.1
15 0.0
20 -2.9 -2.0
25 30

0.0

0.0

0.0

On root of Maple used for Angle pt.

Sta. B.S. H. T. F.S. Elev.

+76		1105	43	4.2	1101.5
126				8.0	1097.7
+15				8.3	1097.4
+20				4.9	1100.8
+45				9.1	1096.6
+80				9.6	1096.1
127				6.2	1099.5
+20				9.2	1098.5
+22				5.8	1099.9
+45				9.8	1095.9
+70				7.1	1098.6
+75				9.0	1096.7
128				9.5	1096.2
T.P.	3.55	1103	88	5.40	1100.33
+61.0				4.5	1099.6
129				4.9	1099.0
B.M.	3.88	1104	35	3.41	1100.48

1677

100.26
101

$\frac{18}{30}$	$\frac{-2.8}{5}$	$\frac{-3.8}{15}$	$\frac{-5.5}{25}$	in creek	
0.0	$\frac{-0.7}{10}$	$\frac{-1.4}{15}$	$\frac{-1.2}{20}$	$\frac{+3.0}{22}$	Level
			0.0		
			0.0		
$\frac{0.0}{30}$	$\frac{+0.8}{10}$	$\frac{+3.2}{15}$	$\frac{+4.1}{25}$	$\frac{+4.0}{30}$	
0.0	$\frac{+1.3}{10}$	$\frac{+1.5}{15}$	$\frac{+2.0}{25}$		
0.0	$\frac{-2.1}{3}$	$\frac{-3.6}{15}$	$\frac{-2.5}{20}$	$\frac{+0.1}{22}$	$\frac{+0.1}{30}$
			0.0		
			0.0		
0.0	$\frac{+1.1}{6}$	$\frac{+2.6}{8}$	$\frac{+3.0}{15}$	$\frac{+3.3}{30}$	
			0.0		
			0.0		
0.0		$\frac{+0.4}{15}$	$\frac{+0.4}{20}$	$\frac{+4.0}{25-30}$	
0.0	$\frac{-1.9}{5}$	$\frac{-3.8}{15}$	$\frac{+2.5}{20}$	$\frac{+1.0}{30}$	$\frac{+3.0}{30}$
0.0	$\frac{+1.0}{10}$	$\frac{-3.1}{15}$	$\frac{-2.8}{20}$	$\frac{-1.1}{30}$	$\frac{+0.7}{45}$

In E. foot, ^{12"} angle about 100' W from line.

Sta BS H. T. F.S. Elev.

130 1104 35 6.9 1097.5

+30 5.3 1099.1

131 8.3 1095.1

132 ^{1096.3} ① 5.9 1098.5

+20 5.9 1098.5

+35 7.9 1096.5

+70 ^{1095.3} ② 8.6 1095.8

133 ^{1099.2} ④ 5.7 1098.7

T.P. 3.61 1103 51 4.5 1099.90

+25 7.2 1096.3

+30 6.8 1096.7

+50 ^{1098.0} ② 9.1 1094.4

134 9.3 1094.2

135 8.8 1094.7

+10 6.5 1097.0

+13 7.7 1095.7

+25 7.7 1095.8

+35 5.0 1098.5

0.0 $\frac{+1.4}{.7} \frac{-0.4}{.5} \frac{-2.2}{.2} \frac{-1.4}{.25} \frac{+0.9}{.3}$

0.0 0.0

0.0 $\frac{+0.5}{.7} \frac{+2.9}{.5} \frac{+3.4}{.25} \frac{+3.5}{.3}$

0.0 $\frac{0.0}{.75} \frac{-2.4}{.17} \frac{-1.1}{.2} \frac{-2.1}{.25}$

0.0 0.0

0.0 0.0

0.0 $\frac{-1.4}{.7} \frac{-1.7}{.75} \frac{+0.3}{.25}$

0.0 $\frac{-6.0}{.5} \frac{-2.5}{.6} \frac{-4.0}{.15} \frac{-2.8}{.2} \frac{-1.5}{.3}$

Dist. to east of 12" Apple about 200' Not 133

0.0 0.0

0.0 0.0

0.0 $\frac{+1.6}{.5} \frac{+3.3}{.15} \frac{+3.6}{.25}$

0.0 $\frac{+3.0}{.5} \frac{+4.0}{.15} \frac{+3.9}{.3}$

0.0 $\frac{-0.5}{.4} \frac{+1.4}{.18} \frac{+2.6}{.15} \frac{+2.6}{.3}$

0.0 0.0

0.0 0.0

0.0 0.0

0.0 0.0

Sta. B.S. H.I. F.S. Elev.

136 1103.51 4.7 1098.8

137 5.8 1097.7

+25 6.7 1096.8

138 7.5 1096.0

+90 6.8 1096.7

139 6.7 1096.8

T.P. 427 1103.03 4.75 1098.76

+50 8.2 1094.8

140 5.4 1097.6

+35 8.0 1095.0

+66.3 6.1 1096.9

B.M. 4.60 1098.43

00

00

$-\frac{0.1}{15}$

$+\frac{0.2}{15}$

00

$+\frac{0.9}{15}$

00

$-\frac{1.6}{15}$

00

00

$+\frac{0.3}{15}$

$+\frac{0.1}{25}$

$\frac{0.0}{35}$

$-\frac{1.0}{12}$ $-\frac{3.1}{14}$ $-\frac{4.1}{15}$ $-\frac{4.0}{25}$ $-\frac{0.6}{30}$

00

$-\frac{1.3}{5}$ $-\frac{2.5}{10}$ $-\frac{3.8}{15}$ $-\frac{3.9}{25}$ $+\frac{0.4}{30}$

3m. W. root 20" pig hickory W. Sta. 141+

10/26/75. R. Hanna
L. Mintern

Sta.	B.S.	H.I.	F.S.	Elev.
B.M.	2.71	11 01 17		1098.43
141			4.9	1096.2
+50			4.4	1096.7
142			3.2	1097.9
+45			5.4	1095.7
+50			7.3	1093.8
143			5.2	1095.9
+80			2.5	1098.6
144			6.2	1094.9
145			6.2	1094.9
146			5.3	1095.8
+50			7.6	1093.5
+55			5.5	1095.6
147			4.3	1096.8
T.P.	2.62	109 9 68	3.08	1097.06
148			3.6	1096.1
+30			3.6	1096.1
+40			5.0	1094.7
+70			6.2	1093.5

Fair-Windy

15'
offset
stakes

±

30' from
offset = 15'
to Pt. of ±

88	$\frac{+0.5}{15}$	$\frac{-2.1}{18}$	$\frac{-3.4}{25}$	$\frac{-3.1}{30}$	$\frac{-4.9}{35}$ Bank
	0.0				
00	$\frac{-1.5}{15}$	$\frac{-2.3}{25}$	$\frac{-4.7}{29}$	$\frac{-5.5}{30}$	
	0.0				
00	$\frac{-3.0}{3}$	$\frac{-3.0}{15}$	$\frac{-1.6}{20}$	$\frac{-0.7}{25}$	
± of old					RR
	$\frac{-3.0}{15}$	$\frac{+0.6}{20}$	$\frac{+1.7}{25}$		
00	$\frac{-2.1}{15}$	$\frac{-0.5}{25}$	$\frac{+1.5}{30}$		
00	$\frac{-0.5}{10}$	$\frac{-2.5}{15}$	$\frac{-2.6}{25}$	$\frac{+0.9}{30}$	
	0.0				
	0.0				
00	$\frac{-2.4}{15}$	$\frac{-3.0}{25}$			
	$\frac{0.0}{15}$	$\frac{-0.7}{25}$	$\frac{-2.8}{30}$		
	0.0				
	0.0				
	0.0				

579

149

1099 68 4.2 1095.5

00 $-\frac{2.2}{3}$ $-\frac{3.7}{15}$ $-\frac{2.1}{25}$ $-\frac{0.4}{25}$ $-\frac{0.9}{30}$

150

7.3 1092.4

00

 $-\frac{0.2}{15}$ $+\frac{1.0}{20}$ $+\frac{2.5}{25}$

B.M.

2.52 1097.16

In N. root 14" Maple 100'S of Barnes line.

+10

6.6 1093.1

00

+15

5.1 1094.6

00

+25

4.5 1095.2

00

 $-\frac{0.2}{15}$ $-\frac{0.7}{25}$ $-\frac{3.1}{38}$

151

5.0 1094.7

00

 $+\frac{0.3}{15}$ $+\frac{0.2}{30}$

152

3.9 1095.8

00

 $\frac{00}{15}$ $-\frac{0.3}{25}$ $-\frac{7.3}{30}$

153

3.6 1096.1

00

 $-\frac{0.5}{15}$ $-\frac{1.7}{30}$

T.P.

2.72 1099.34 3.06 1096.62

154

5.0 1093.7

00

 $+\frac{0.4}{15}$ $+\frac{1.0}{25}$ $+\frac{1.0}{30}$

155

5.1 1094.2

00

 $\frac{00}{15}$ $-\frac{0.2}{30}$

+5

5.5 1093.8

00

+8

6.8 1092.5

00

+15

6.6 1092.7

00

 $-\frac{1.9}{15}$ $-\frac{2.0}{30}$

+20

6.6 1092.7

00

+23

4.8 1094.5

00

+35

5.1 1094.2

00

 $+\frac{0.3}{15}$ $+\frac{1.2}{30}$

15.9 1098.49 6.2 1092.3

160 6.9 1091.6

+30 5.6 1092.9

+35 8.0 1090.5

+80 7.0 1091.5

+85 4.8 1093.7

161 8.5 1090.0

162 5.7 1092.8

T.F. 2.57 1098.06 3.00 1095.49

163 4.1 1094.0

+85 6.2 1091.9

164 4.5 1093.6

+65 7.6 1090.5

+70 7.7 1090.4

B.M. 0.23 1097.83

165 7.0 1091.1

+60 7.0 1091.1

+85 5.1 1093.0

00

00

00

00

00

00

00

00

00

00

00

00

00

+0.9
15

+1.5 +2.1
15 30

+0.9
15

+2.6 +2.1
20 30

+1.6 +1.1 +4.3
5 10 15

+2.0
15

+4.1
30

+2.6
30

+0.4
15

-0.7
10

0.0
15

-0.8
15

+1.0
10

+1.7
15

00

+0.2
30

+1.3
30

-0.8
30

+1.6
30

U.S.G.S. tablet on S.W. parapet.

-2.0
15

-2.4
25

00

00

cloudy 10/27/15
still a.m.

B.M.	4.87	1096.47		1091.60
17.6			5.7	1090.8
177			7.1	1089.4
178			8.8	1087.7
T.P.	4.56	1095.16	5.87	1090.60
²⁰ +26.5			4.4	1090.8
+75			7.3	1087.9
+80			4.5	1090.7
179			6.0	1089.2
+15			5.2	1090.0
+18			6.6	1088.6
+25			7.8	1087.4
+30			6.5	1088.7
+35			4.3	1090.9
+50			4.8	1090.4
+65			5.9	1089.3
+67			8.3	1086.9
+70			6.6	1088.6

F. Hanna
L. Mintern

B.M. on E. root of large snag	150' N.	175		
00	-2.2	-2.5	-1.5	
	15	25	30	
00	⁰⁰ 10	-2.2	-1.9	+0.8
		15	15	20
00		+0.2	+2.7	+2.8
		15	25	30
00	⁰⁰ 7	-2.8	-3.6	-2.8
		12	15	25
				⁰⁰ 30
			00	
			+1.3	+1.2
			15	25
				-0.3
			0.0	30
			0.0	
			0.0	
			+0.4	-0.1
			15	30
			0.0	
			0.0	
			+0.2	+0.5
			15	30
			0.0	
			0.0	
			-1.1	-0.1
			15	20
				+0.5
				30

Sta. B.S. H.I. F.S. Elev.

180 1095.16 5.3 1089.9

+55 7.0 1088.2

181 6.8 1088.4

+25 7.0 1088.2

+30 8.1 1087.1

+75 6.3 1088.9

T.P. 3.10 1093.28 4.93 1090.13

182 4.1 1089.2

+25 6.5 1086.8

+30 3.9 1089.4

+35 5.4 1087.9

183 5.4 1087.9

184 3.1 1090.2

+38 4.4 1088.9

T.P. 4.06 1093.22 4.12 1089.16

B.M. 3.44 1089.78

+70 4.6 1088.6

+80 5.6 1087.6

+85 7.1 1086.1

00 $\frac{-2.0}{15}$ $\frac{-2.2}{25}$ $\frac{+0.3}{30}$

00 $\frac{-1.6}{15}$ $\frac{00}{20}$ $\frac{+1.5}{30}$

00 $\frac{+0.8}{15}$ $\frac{+0.7}{30}$

00

00

00 $\frac{-0.2}{15}$ $\frac{-2.1}{18}$ $\frac{-3.1}{25}$ $\frac{-0.2}{30}$

00 ~~2.1~~ $\frac{-3.2}{15}$ $\frac{-2.1}{25}$ $\frac{0.0}{30}$

00

00

00 $\frac{+0.5}{15}$ $\frac{+0.8}{30}$

00 $\frac{-0.3}{15}$ $\frac{+1.1}{25}$ $\frac{+1.0}{30}$

00 $\frac{-1.5}{15}$ $\frac{-3.0}{30}$

00 $\frac{-1.2}{15}$ $\frac{-0.4}{25}$ $\frac{-0.1}{30}$

W. root 14" Staple 75' E. of 184+38

00 $\frac{-0.3}{15}$ $\frac{-0.3}{30}$

00

00

Sta	B.S.	H. I.	F.S.	Elev					
185	1093.22		6.6	1086.6	00		$\frac{-1.5}{15}$	$\frac{-1.1}{25}$	$\frac{+0.1}{30}$
186			5.3	1087.9	00	$\frac{-1.2}{3}$	$\frac{-2.6}{5}$	$\frac{-2.2}{13}$	$\frac{-1.0}{15}$
+21			5.1	1088.1	00	$\frac{-0.9}{7}$	$\frac{-2.7}{9}$	$\frac{-3.6}{15}$	$\frac{-3.6}{25}$
187			8.5	1084.7	00		$\frac{0.0}{15}$	$\frac{+1.3}{25}$	$\frac{+2.8}{30}$
188			6.0	1087.2	00	$\frac{+0.6}{10}$	$\frac{-2.1}{12}$	$\frac{-1.5}{15}$	$\frac{-1.4}{30}$
T.P.	2.93	1091.30	4.85	1088.37					
+29			3.3	1088.0	00	$\frac{-1.0}{10}$	$\frac{-2.4}{15}$	$\frac{-2.9}{30}$	
189			3.5	1087.8	00	$\frac{-2.0}{3}$	$\frac{-3.2}{15}$	$\frac{-3.0}{30}$	
190			5.7	1085.6	00		$\frac{-1.0}{15}$	$\frac{-1.4}{30}$	$\frac{0.2}{35}$
+17.6			3.8	1087.5	00	$\frac{-0.6}{5}$	$\frac{-2.2}{7}$	$\frac{-3.1}{15}$	$\frac{-2.9}{30}$
191			5.5	1085.8	00	$\frac{-0.1}{9}$	$\frac{-1.3}{11}$	$\frac{-1.8}{15}$	$\frac{-2.0}{25}$
192			3.7	1087.6	00	$\frac{-0.8}{7}$	$\frac{-1.8}{10}$	$\frac{-2.3}{15}$	$\frac{-1.5}{25}$
193			3.8	1087.5	00	$\frac{-0.5}{7}$	$\frac{-3.5}{10}$	$\frac{-3.1}{15}$	$\frac{-2.5}{30}$
T.P.	3.20	1091.49	3.01	1088.29					
+37			3.7	1087.8	00	$\frac{-1.2}{7}$	$\frac{-2.9}{10}$	$\frac{-3.5}{15}$	$\frac{-2.8}{25}$
194			4.2	1087.3	00	$\frac{+0.2}{10}$	$\frac{-2.4}{15}$	$\frac{-2.5}{25}$	$\frac{+0.2}{35}$
+50			7.3	1084.2	00		$\frac{-0.2}{15}$	$\frac{+1.1}{25}$	bank
195			7.8	1084.7	00		$\frac{+0.1}{15}$	$\frac{-0.1}{25}$	$\frac{+1.1}{35}$

Lags, brush & debris.

Sta	B.S.	H. I.	F.S	Elev
196		1091.49	6.4	1085.1
B.M.	2.93	1091.86	2.56	1088.93
+15			8.7	1083.2
197			8.7	1083.2
198			8.9	1083.0
199			8.9	1083.0

00

$$\begin{array}{r} -1.1 \\ -7.5 \\ \hline -8.6 \\ -0.7 \\ -2.5 \\ \hline -9.3 \\ +0.1 \\ \hline -9.2 \end{array}$$

On E. root 12" beech 60' Lt 195470

00

9 100' down stream

9 200' " " "

9 300' " " "

Assumed on Relocated Line.

Sta.	Elev.
191	1084.0
192	1087.6
193	1087.5
194	1087.0
+75	1083.2

Check Levels
on Lat. #3

Sta	B.M.	1126	18	F.S.	1122.69	16	1122	72	0.3H	7.67	15.05
0			0.2 high	6.78	20.00	17			0.1H	7.97	14.75
1			✓	6.99	19.69	18			0.2H	8.28	14.44
2			0.2 high	6.80	19.30	19			0.3H	8.59	14.03
3			0.1 high	7.11	19.07	20			0.3H	8.90	13.82
4			0.1 high	7.42	18.76	21			0.3H	9.21	13.51
5			0.1 high	7.73	18.45	22			0.5H	9.49	13.23
6			0.1H	8.03	18.15						
7			✓	8.34	17.84						
8			✓	8.65	17.53						
9			✓	8.96	17.22	B.M.	289	1121	17		1118.28
10			0.1H	9.27	16.91	51			0.3H	8.09	13.13
11	—		0.3H	9.58	16.60	52			0.1H	8.27	12.90
12	—		0.3H	9.89	16.29	53			0.2H	8.49	12.68
B.M.				5.41	1120.77	54			0.2H	8.72	12.45
T.P.	2.51	1122	72	5.97	1120.21	55			0.2H	8.94	12.23
13	—		0.1H	6.77	15.95	56			0.1H	9.17	12.00
14	—		0.5H	7.05	15.67	T.P.	27.5	1120	0.3	389	1119.28
15			0.2H	7.36	15.36	57			0.3H	8.27	11.76
						58			0.4H	8.51	11.52

ON MAIN DITCH

	1120	03				54	35	1117	53	F.31	Elev.
59		✓	8.75	11.25	76			0.1H	10.33	07.20	
60		✓	8.99	11.54	77			0.1H	10.57	06.96	
61		✓	9.23	10.30	78			0.2H	10.81	06.72	
62		✓	9.47	10.56	79			0.1H	11.05	06.45	
63		0.2Low	9.71	10.32	80			0.3Low	11.29	06.24	
64		0.1Low	9.95	10.08	81			0.3H	11.53	06.00	
65		0.2Low	10.19	09.84	82			0.3H	11.77	05.76	
T.P.	358	1117	53	605	1113.95	T.P.	291	1113	87	6.57	1110.86
66		✓	9.73	09.60	83			0.2H	8.35	05.52	
67		✓	8.87	09.36	84			0.3H	8.59	05.28	
68		0.3Low	8.41	09.12	85			0.1H	8.83	05.04	
69		0.2Low	8.65	08.88	86			✓	9.07	04.80	
70		✓	8.89	08.64	87			Water too deep	9.31	04.56	
71		0.2Low	9.13	08.40	88			0.1H	9.55	04.32	
72		✓	9.37	08.16	89			✓	9.79	04.08	
73		✓	9.61	07.92	90			0.1H	10.03	03.84	
74		0.2Low	9.85	07.68	91			0.5H	10.27	03.60	
75		✓	10.09	07.44	92			0.1H	10.51	03.36	
76					93						

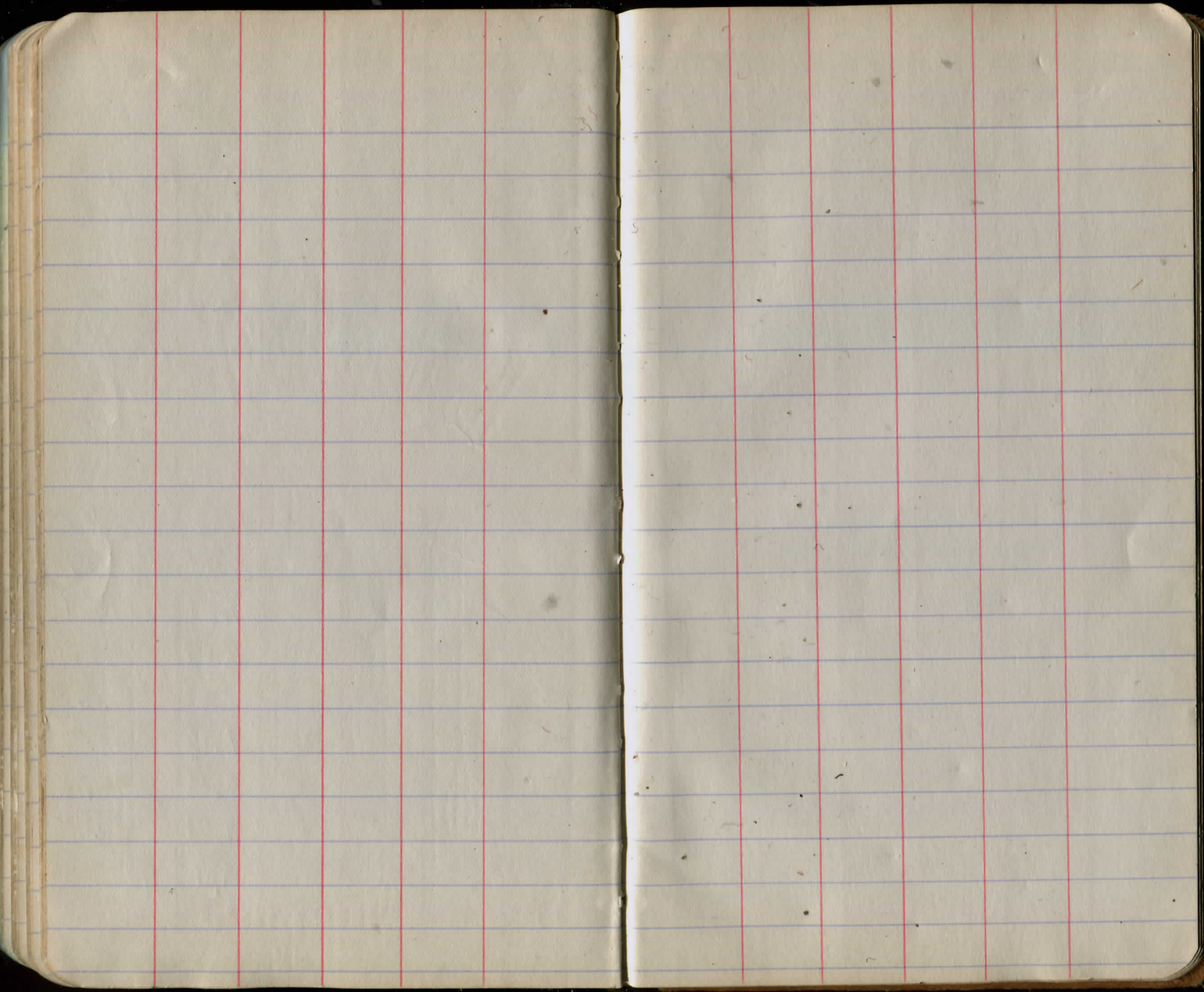
B.M.	5.76	1124	04		1118.28
50			o.1H	10.68	13.36
49			o.2Low	10.46	13.58
48			✓	10.23	13.81
47			✓	10.00	14.04
46			o.2H	9.78	14.26
45			o.2H	9.55	14.49
44			o.1H	9.33	14.71
43			✓	9.10	14.94
42			o.3Low	8.87	15.17
T.P.	6.45	1124	41	6.08	1117.96
41			✓	9.02	15.39
40			o.2H	8.79	15.62
39			o.2Low	8.56	15.85
38			✓	8.34	16.07
37			✓	8.11	16.30
36			o.1H	7.89	16.52
35			o.1H	7.66	16.75
34			o.2Low	7.43	16.98

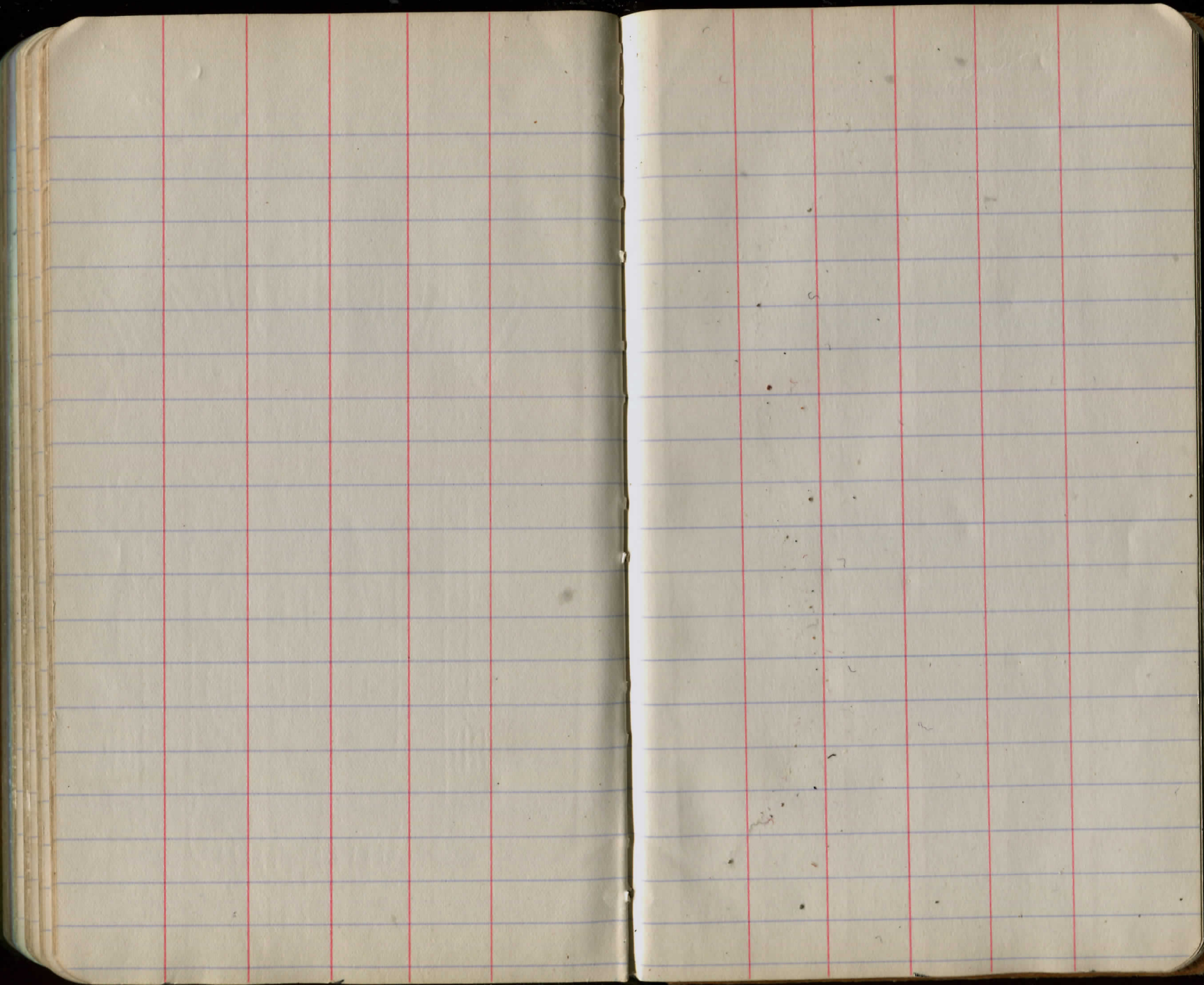
1124 41

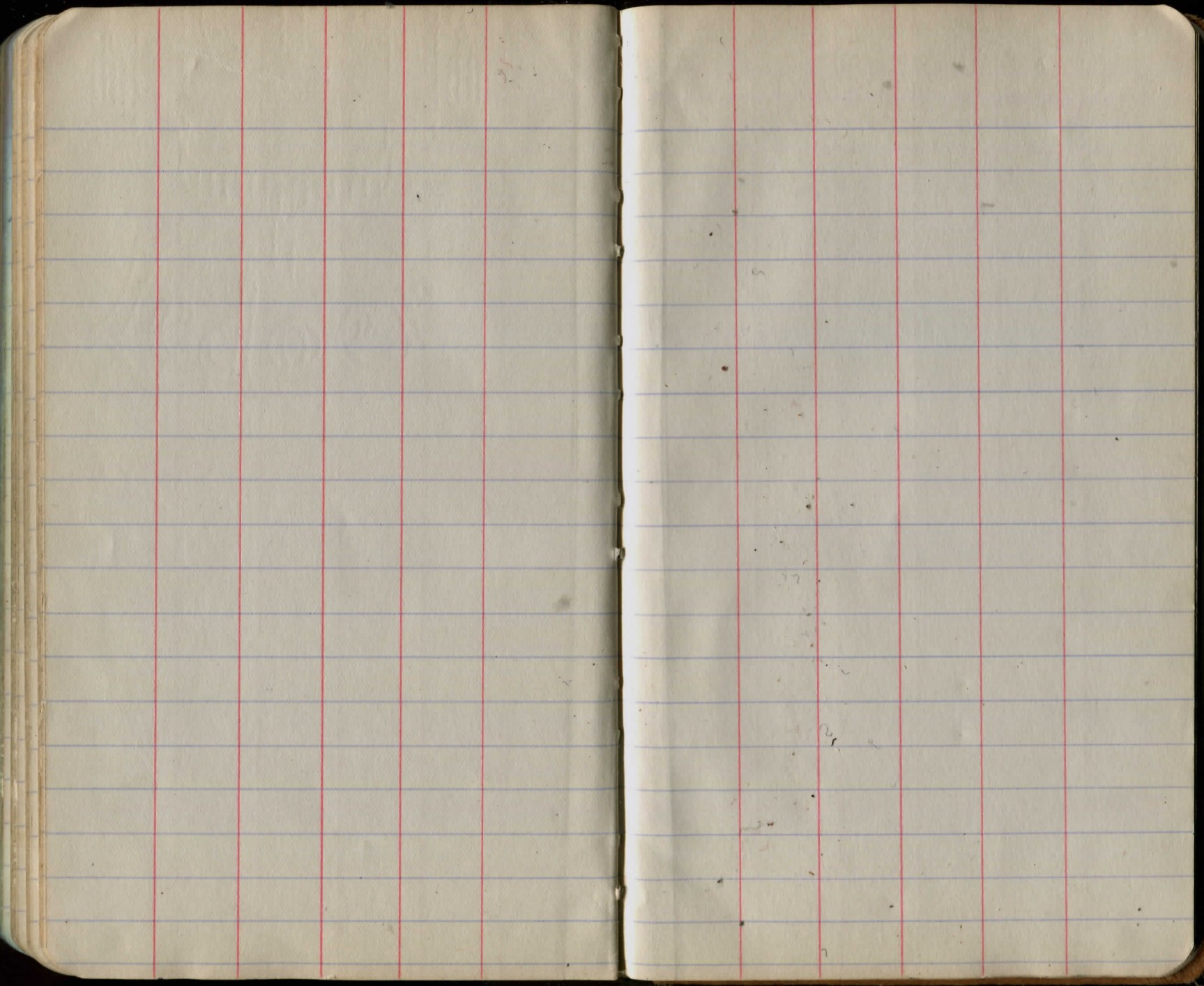
33			o.2Low	7.21	17.20
32			✓	6.99	17.42
31			o.1H	6.76	17.65
30			o.1H	6.53	17.88
T.P.	7.70	1124	15	2.96	1121.45
29			✓	11.04	18.11
28			✓	10.82	18.33
27			✓	10.59	18.56
26			✓	10.36	18.79
25			o.2H	10.14	19.01
24			✓	9.91	19.24
23			o.1Low	9.69	19.46
B.M.					19.69
22			✓	9.46	19.69
21			✓	9.23	19.92
20			✓	9.01	20.14
B.M.				437	1124.78
19			o.3Low	8.78	20.37
18			o.1H	8.55	20.60

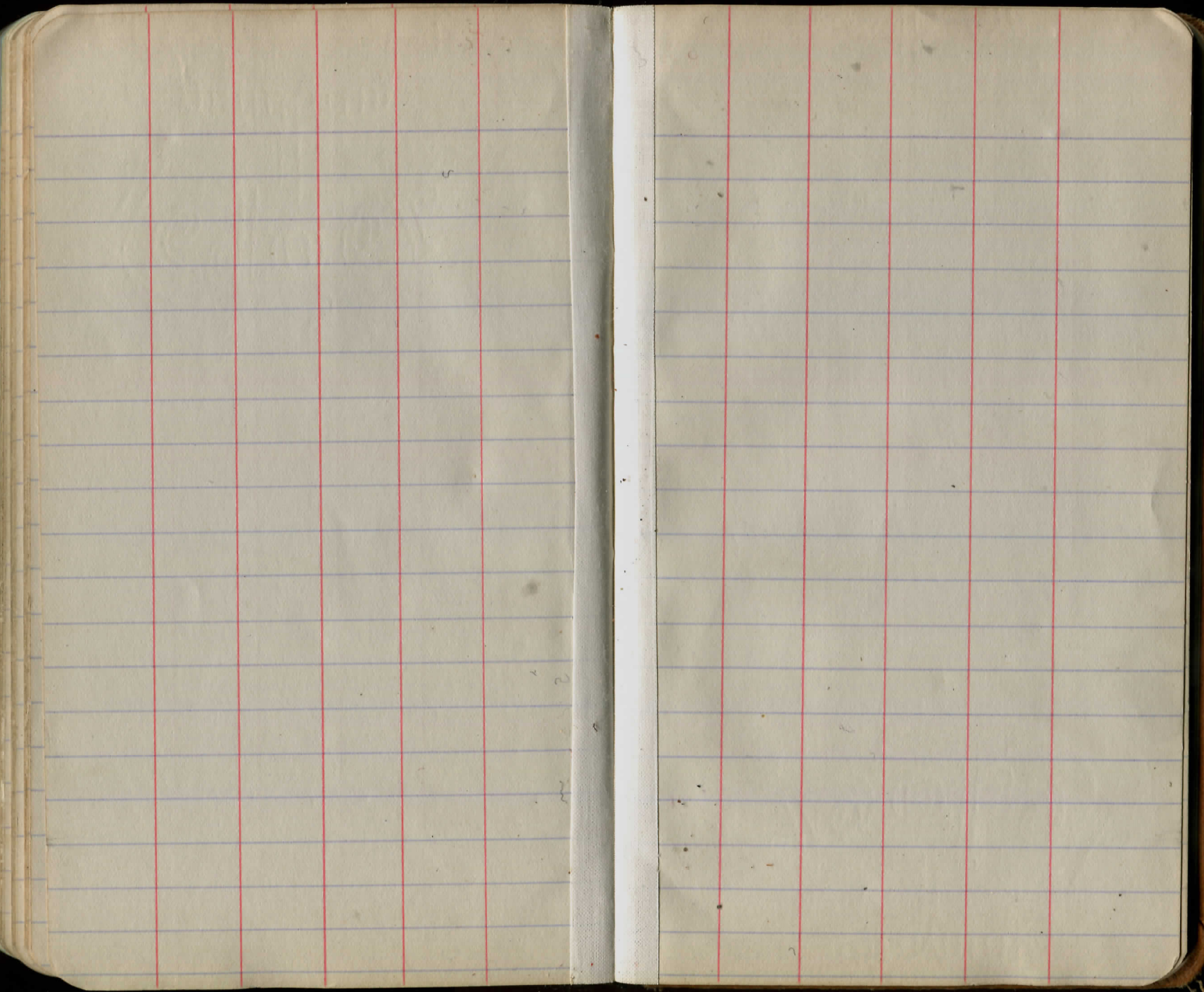
1129 / 15

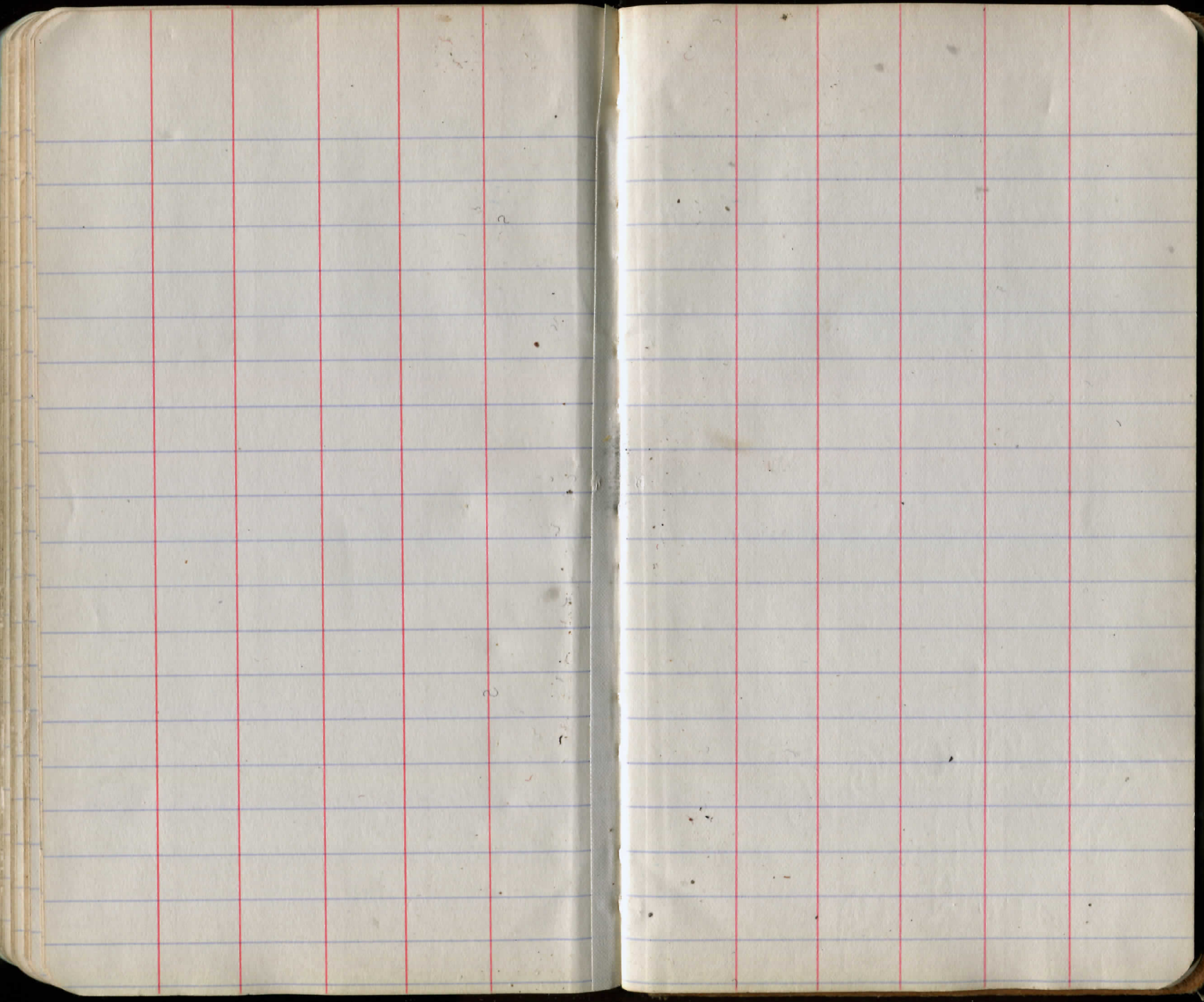
17		←	8.33	20.82	
16		←	8.10	21.05	
T.P.	8.89	1134	33	371	1125.44
15		←	13.06	21.27	
14		o.H.	12.83	21.50	
13		←	12.22	22.11	
12		o.H.	11.61	22.72	
11		←	11.01	23.32	
10		←	10.40	23.93	
9		o.R.H.	9.79	24.54	
8		←	9.19	25.14	
7		o.H.	8.58	25.75	
6		←	7.97	26.36	
5		oA Low	^{7.50} 7.37	26.96	
4		oLow	^{6.9} 6.76	27.57	
3		o2 Low	6.15	28.18	
2		←	5.54	28.79	
1		o.H.	4.94	29.39	
0		o2 H.	^{4.1} 4.33	30.00	

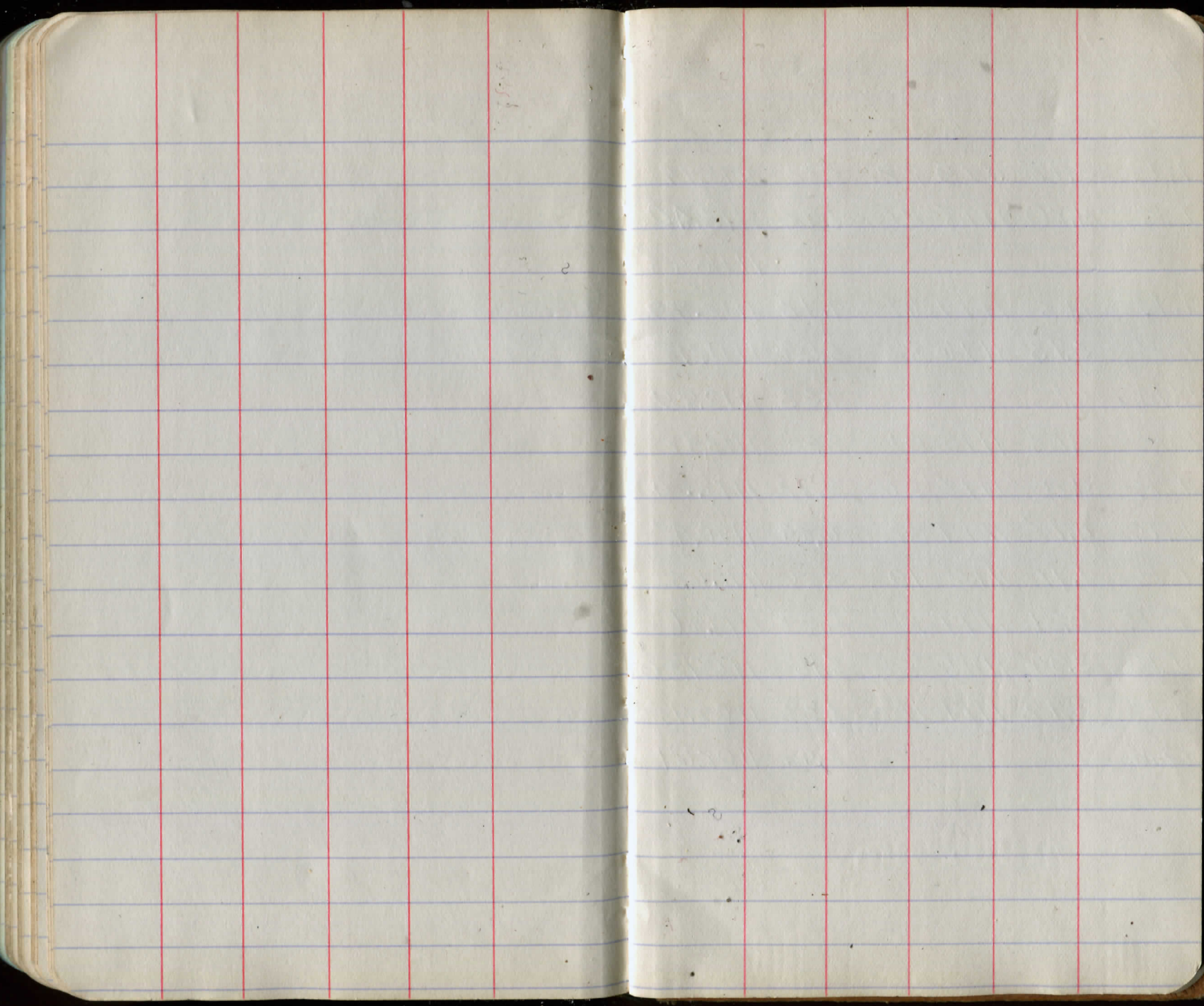












7/30/14

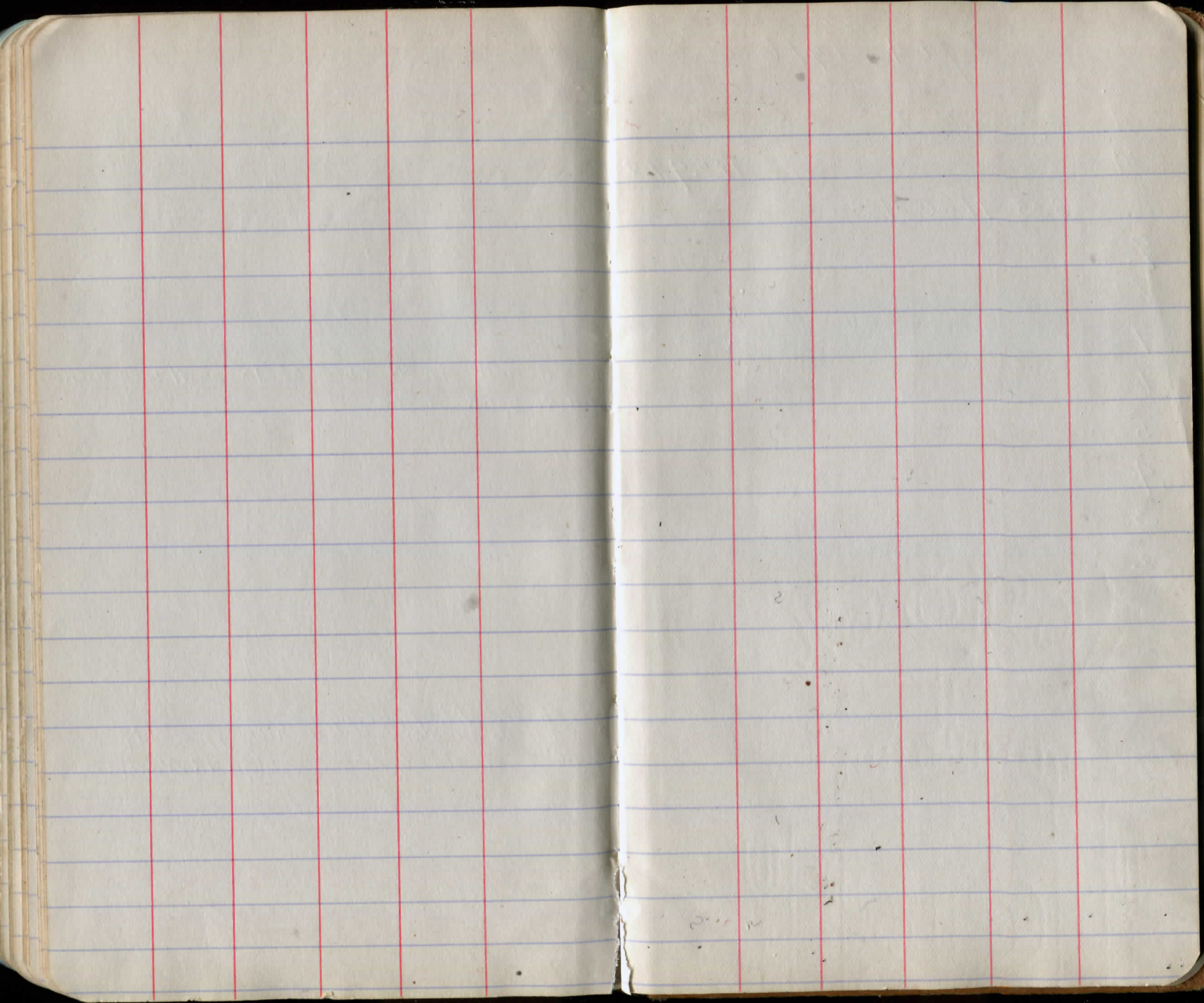
F. J. ...
P. ...

warm-cloudy

sta	BS	N	T	F.S	Elev.
T.P.	3.48	1119	22	5.82	1115.74
T.P.	4.80	1118	20	1.72	1113.40
					1116.48
T.P.	1.13	1117	61	4.72	1112.89
T.P.	3.93	1116	82	5.04	1111.78
B.M.				4.33	1112.99
T.P.	4.13	1115	91	2.45	1113.96
T.P.	4.80	1118	26	5.72	1112.54
T.P.	4.78	1117	32	6.84	1110.48
T.P.	4.71	1115	19	3.56	1111.63
T.P.	5.51	1117	14	5.54	1111.60
T.P.	3.94	1115	54	8.15	1107.30
T.P.	3.72	1111	11	8.33	1102.78
B.M.				2.44	1108.67

2-8d nails in W root of 18" shell bark hickory
on W bank Sta

Creek bed N. of bridge
2-8d nails in S. root of 16" hickory. 300' N of Rd.
200' E of old creek bed (on P. Weaver)

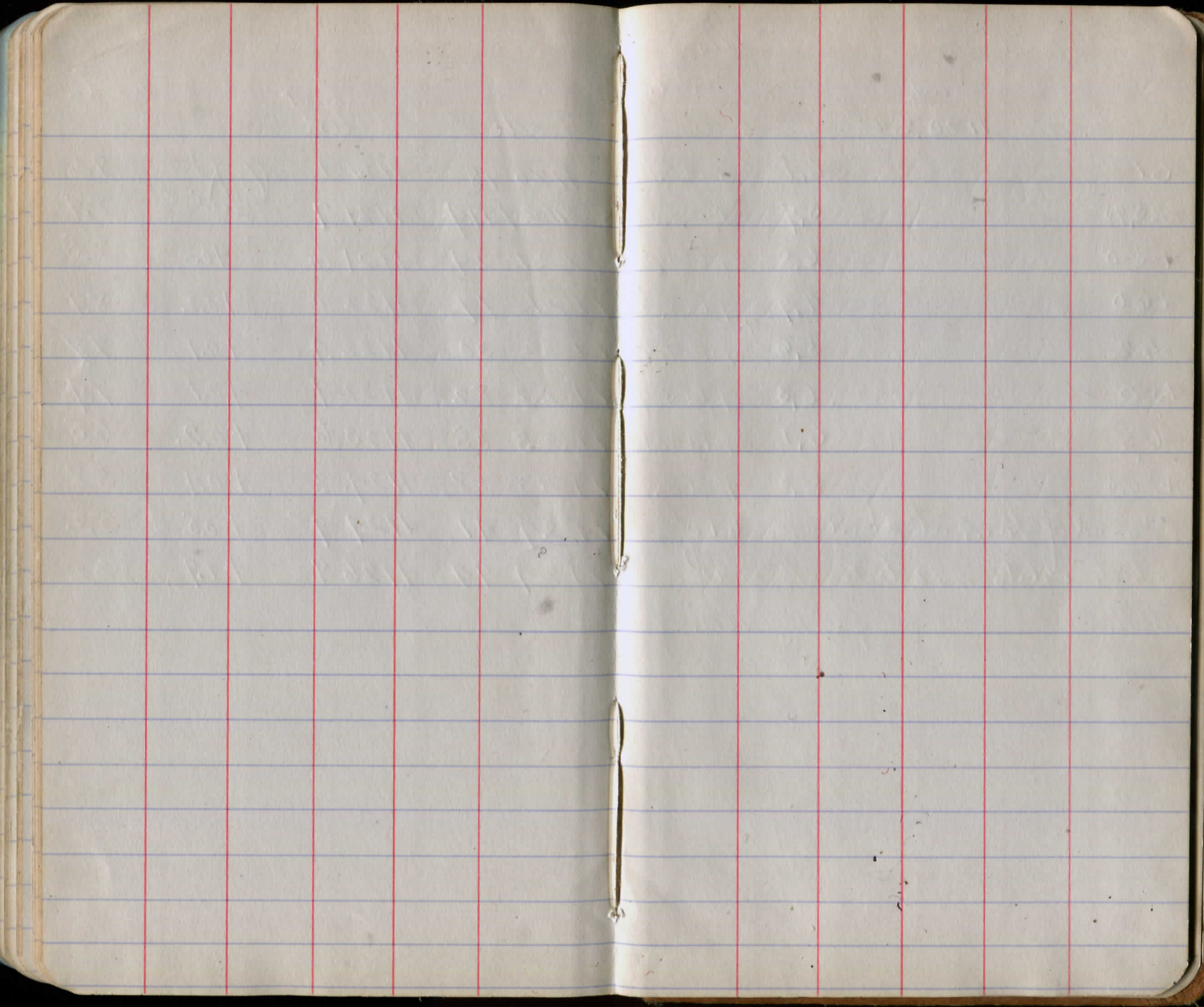


Sept 4 - 1916

BM	BS	HI	FS	elr
BM				1129.78
	535	1130	13	
9				
8				
7				
6				
5				
4				
3				
2				

Grade	present elr.	rod
1120 18	1121.1	9.0
96 1120 71	1121.7	8.4
1121 24	1121.6	8.5
1121 77	1122.0	8.1
1122 30	1122.4	7.7
1122 82	1122.7	7.4
1123 35	1123.6	6.5
1123 88	1124.3	5.8
1124 41	1124.9	5.2
1124 99	1126.9	3.2

D. N. Hill Jr



Kenny + Pindler
April 16th - 1915

A.D.

+B.S. 1120.22 -FS Elev

61	6.1	1114.1
+25.75	3.9	1114.3
+5.0	6.0	1114.2
+6.0	4.9	1115.3
62	5.6	1114.6
+5.0	6.3	1113.9
63	6.1	1114.1
+36.5	6.3	1113.9

" end of line A at station 61 of
which adds 236.5' length of line

B.M. -4.945 1115.28

Left

2

Right

$\frac{+1.0}{15.}$	$\frac{+0.6}{8.0}$	$\frac{+0.2}{4.0}$	$\frac{+.3}{2.0}$	$\frac{0.0}{2.0+0}$
$\frac{+1.5}{15.}$	$\frac{+0.13}{12.}$		$\frac{+0.4}{5.0}$	$\frac{+0.9}{18.}$

same R. & h. for 15' from L

average R. & L " " "

" " " "

" " " "

" " " "

" " " "

old line

6:10 clock P.M.

as first located.

Checked on P.M.

Friday April 16th 1915 - E. Keeney assist
 Relocation beg. at 31st 45

	+88	140	-7.8	class.
B.M.	+2.26	1122.32		1120.06
45			4.4	1117.9
+50			5.7	1116.60
46			4.9	1117.4
+50		" 0.8	5.5	1117.62
				1116.8
+80			5.5	1116.5
+85			4.0	1118.3
47			4.1	1118.2
+75			5.5	1116.8
+90			4.9	1117.4
48			4.2	1118.1
+50			5.4	1116.9
+65			4.4	1117.9
+80			5.2	1117.1
+90			6.2	1116.1
49			6.1	1116.2
+10			4.4	1117.9
+80			5.3	1117.0
50			5.9	1116.4

Left	±	Right
	0	
25' E of sta. 48+40		
15'		+1.0
same		15'
-1.0		+1.0
15'		15'
+1.0		0.0
15'		15'
0.0		0.0
15'		8
same R+L		15'
" " "		"
" " "		"
+1.0		-1.0
15'		15'
same R+L		15'
" " "		"
+1.0		-2.0
15'		15'
same R+L for 15'		"
" " "		"
" " "		"
" " "		"
" " "		"
-0.8		+0.7
15'		15'

	+BS	H.S.	-F.S.	Elevs	L.	R	B
50+10	1122.320		6.2	1116.1	same for 10-		R + L of E
+25			5.3	1117.0	"		"
+70			5.1	1117.2	"		"
5-1			5.7	1116.6	"		"
+45			6.1	1116.2	"		"
+50			7.2	1115.1	"		"
+70			6.6	1115.7			
+75			5.9	1116.4			
5-2			6.4	1115.9			
+30			6.9	1115.4	$\frac{-1.0}{15}$		$\frac{+0.6}{15}$
TP			-4.625	1117.695	Top of stake 5-2		

	+BS	H.S.	-F.S.	Elevs	L.	R	B
+40	1121.200	meter 0.3	6.0	1115.5 1115.2	same R + L		for 15' $\frac{+1.1}{15}$
5-3			6.2	1115.0	"		"
+10			5.3	1115.9	$\frac{-1.1}{15}$		same 15'
+50			6.3	1114.9	same for 10-		"
+60			5.1	1115.1	"		"
5-4			5.4	1115.8	average R + L		"
+35			6.3	1114.9	$\frac{+1.0}{15}$		$\frac{-1.4}{15}$
+70 ^{avg}			7.3	1115.9	average		for 15'

	+FS	40	-FS	
5-5		1121.200	6.5	1114.7
+50			7.5	1113.7
56			6.8	1114.2
5-6			6.2	1115.0
+15			5.8	1115.9
+25			4.9	1116.3
57			5.2	1116.0
+45			5.1	1116.1
+50			6.5	1114.7
58			6.2	1115.0
+10			6.4	1114.8
+20			7.3	1113.9
+50			6.5	1114.7
59	water	0.0	6.5	1114.7
TP		22	-5.08	1116.12
	+410	1120.22	-6.9	1113.3
+50			6.9	1113.3
+75			7.1	1113.1
60			6.0	1114.2
60	surface of water		5.5	1114.7

	LT.	R	R ₁
	$\frac{71.4}{15}$		$\frac{-1.1}{15.0}$
	same for 10-R + L		$\frac{0.6}{15}$
	$\frac{+2.4}{15}$ $\frac{70.5}{8}$		
	surface water		$\frac{-1.7}{15}$
	$\frac{+1.0}{10+15}$ $\frac{+1.2}{2}$		
	same R & L	for 15'	
	" " "	" "	
	" " "	" "	
	" " "	" "	
	$\frac{+1.0}{15}$ $\frac{+0.8}{5.0}$		
	$\frac{+1.4}{10+15}$ $\frac{3.0}{8}$		
	$\frac{+1.8}{15}$ $\frac{+2.0}{8}$		
	$\frac{-1.0}{15}$		$\frac{+1.5}{15}$
	$\frac{+1.0}{15} - \frac{1.2}{10}$		$\frac{+0.4}{15}$
	E root of elm about 2' R 58+75		
	same R & L	15'	
	"	"	
	$\frac{+0.6}{15}$		$\frac{-1.0}{15}$
	water surface		→ Back 6 pages

Friday March 26th 1915
Fidler & R Hanna

	+BS	H.S.	-T.S	Elevations
BM 89 ⁺ 40	4.07	1124 13	-	1120.06
T.O.	+1.98	1120.06	-6.05	1119.08
BM 81 ⁺ 60			-4.78	1115.29
BM 81 ⁺ 62 ⁺ 40 T.P.	+3.74	1118 50	-5.20	1115.06
T.O.	+2.84	1117 04	-3.70	1114.70
T.O. BM Hickney	+2.91	1114 72	-5.23	1111.81
			-1.45	1113.27

Run first lateral to
 patches line noting
 property line between
 Leonard & Butterfield
 This will be open ditch.

Run second lateral
 from main ditch, using the
 center of the bridge as a pivot,
 using what is possible of the
 ditch as now dug on Patches,
 at least do not get center
 of new ditch more than
 20 or 25 ft from center of old
 so that the dirt from the new
 will fill the old. Run this
 lateral to south thru wood to
 Atwoods line fence (none)
 Do not put in section running
 off east at all. Open ditch.

79	79	76	76	73	73	73
3.6	3.4	4.1	4.8	3.4	5.8	2.9
2.3	4.1	1.4	7.6	3.9	1.5	4.4
1.1		4.6		7.5		
5.8				5.4		
		4.25	8.75			
7.0		4.80	4.35			
		9.05	4.40			
		1102.90				
		1111.95	8.75			
sl 0		8.45	6.85			
		2.40	1.60			
		6.00				

- 2.80 maple tree near line

197		90.65	
172		1085.92	
23	4.73	4.73	
147	25	1892.	57
	228		
	200		
	250		
	225		
	50		
1096.16			
45.68			
48			
1095.16			
52			
1099.73			
95.08			
4.65			

207
 16
 1120.03
 608
 1113.95



924.8
 26.18
 170
 20.75
 1095.08
 90.65
 9.43
 4.73
 9.16
 1105.30
 99.73
 5.57
 109389
 362
 108977

60+45 P.L.1
 2272
 2087
 1.95
 26.18
 5.17
 20.21

Run first lateral to
 patches line noting
 property line between
 Omond & Butterfield
 This will be open ditch.

Run second lateral
 from main ditch, using the
 center of the bridge as a pivot
 using what is possible of the
 ditch as now dig on Patches
 at least do not get center
 of new ditch more than
 20 or 25 ft from center of old
 so that the dirt from the new
 will fill the old. Run this
 lateral to south three rods to
 Atwoods line fence None
 do not put in section running
 off east at all. Open ditch.

79	79	76	76	73	73	73
2.2	3.4	4.5	4.8	3.4	5.8	2.9
2.3	4.4	3.1	4.6	3.9	1.5	4.4
1.1		1.5	7.6			
2.8		4.6		5.4		
		4.25	8.75			
7.0		4.80	4.36			
		9.05	4.40			
		1102.90	8.55			
		1111.95	6.85			
sls 0		8.45	1.60			
		2.40				
		6.00				

- 2.80 maple on near line

197
 172
 25 4.73
 147 25
 223
 200
 250
 225
 50
 1096.16
 11.08
 48
 1095.16
 52
 10 99.73
 95.08
 4.65
 2.3
 5
 1120.03
 608
 113,95

90.65
 1085.92
 4.73
 1892. 57
 26.18
 170
 20.75
 1095.08
 90.65
 4.43
 4.73
 9.16
 1105.30
 99.73
 5.57



60+45 P.L.
 22.72
 20.27
 4.95
 26.18
 5.17
 20.21

DIETZGEN



TRADE MARK

GIBBS